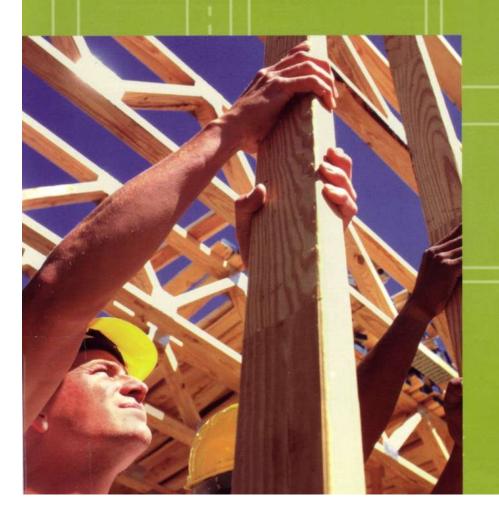
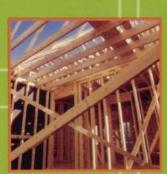
THE ESSENTIAL GUIDE TO FRAMING





- **√** JOISTS
- **√ TRUSSES**
- **√ WALLS**
- ✓ AND MORE

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Estimating Materials

Converting Linear Feet to Board-Feet

Formula method. To find board-feet, multiply the total length (in ft.) by the nominal lumber thickness by the width (in in.), and then divide the total by 12. For example: (10) 8-ft. $2x4s = (80 \times 2 \times 4) \div 12 = 53.3$ board-feet

$$(L \times T \times W) \div 12$$

Factor method. Alternatively, use the conversion factors in Figure 1.

Floors and Ceilings

Estimating Number of Joists

To calculate the number of joists, use the formulas shown in **Figure 2** for the appropriate on-center spacing.

Estimating Rim Joists

Remember to include rim stock in the total joist count. Rim joist stock is calculated as follows:

BUILDING LENGTH (FT.) x 2/ Lumber Length

Figure 1. Linear Feet to Board-Feet Conversion

Nominal Lumber Size	Conversion Factor	
1x4	.33333	
1x6	.50000	
1x8	.66667	
1x10	.833333	
1x12	1.00000	
2x3	.50000	
2x4	.666667	
2x6	1.00000	
2x8	1.33333	
2x10	1.66667	
4x4	1.33333	
4x6	2.00000	
6x6	3.00000	

As an alternative method of calculating board-feet, multiply the lin. ft. of each lumber size you are using by the corresponding conversion factor. Example: (10) 8-ft. 2x4s = 80 x .666667 = 53.3 board-feet

Lumber lengths should be multiples of the o.c. spacing. For example, use 12s, 16s, 20s, etc., for 16-in. o.c. joist spacing. Depending on the length of the building, it may be more efficient to count these individually, mixing lumber lengths that break evenly on the joists.

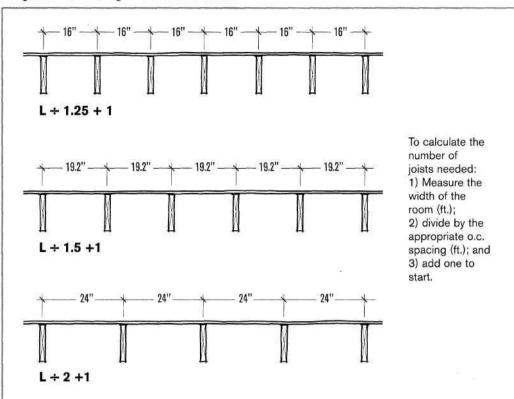


Figure 2. Estimating Joists and Rafters

Estimating Subflooring

The most accurate method of estimating subflooring is to graph scaled lines over the floor plans in 4x8-ft. increments. For a quick alternative, calculate as follows:

- For each section of subfloor, square off any jogs or cantilevers from the outside perimeter on the plans to form one large perimeter rectangle.
- For each section, multiply the length by the width of the perimeter rectangle.

• Divide by 32 (for 4x8 panels).

Remember to add a couple of sheets to the total panel count to accommodate cutting error and waste, especially if there are jogs in the floor plan.

Walls

Estimating Plate Stock

Order wall plates in a quantity that's at least four times the total length of the walls. On walls that run in the same direction as the trusses or joists, an additional plate is needed for drywall backing at the ceiling. More will be needed to cover waste, miscellaneous backing, and continuous fire blocking for walls over 8 ft. high.

Estimating Studs

For a small house (less than 2,000 sq. ft.) with 16-in. o.c. framing, order 1 stud for each lin. ft. of wall framing — both interior and exterior. For a larger house framed 16 in. o.c., order 1.25 studs for each lin. ft. of wall framing.

Estimating Headers

In a house with windows under 36 in. wide, use the following shortcuts:

For solid-sawn headers:

- Count the number of windows and doors; count French doors or sliders as 2;
- 2) Divide by 3 and order that many 10-footers.

For doubled-2x headers:

1) Count the number of windows and

- doors; count French doors or sliders as 2;
- 2) Multiply by 2;
- 3) Divide by 3 and order that many 10-footers.

For extra large or extra narrow windows, calculate headers individually.

Estimating Wall Sheathing

For rectangular wall areas:

Wall Area = Total Wall Length x
Wall Height

SHEATHING (4x8 PANELS) = WALL AREA ÷ 32

- Multiply the total length of exterior walls by the wall height to get total wall area;
- 2) Subtract the areas of major openings such as sliders or large windows;
- 3) Divide by 32 (for 4x8 panels).

Remember to account for gable-end walls.

For regular gables (same pitch both sides of ridge):

Multiply span by total rise. This gives you the total for two gable-ends.

For irregular gables or single gableend walls:

- 1) Multiply total run by total rise for each gable end;
- 2) Divide by 32.

Figure 3. Rafter Line Length (LL) Ratios

Roof Pitch/12	COM LL Ratio	H/V LL Ratio
1	1.0035	1.4167
1 ¹ /2	1.0078	1.4197
2	1.0138	1.4240
21/2	1.0215	1.4295
3	1.0308	1.4361
31/2	1.0417	1.4440
4	1.0541	1.4530
41/2	1.0680	1.4631
5	1.0833	1.4743
51/2	1.1000	1.4866
6	1.1180	1.5000
61/2	1.1373	1.5144
7	1.1577	1.5298
71/2	1.1792	1.5462

Pitch/12	Ratio	Ratio
8	1.2019	1.5635
81/2	1.2254	1.5817
9	1.2500	1.6008
91/2	1.2754	1.6207
10	1.3017	1.6415
10 ¹ /2	1.3288	1.6630
11	1.3566	1.6853
11 ¹ /2	1.3851	1.7083
12	1.4142	1.7321
14	1.5366	1.8333
16	1.6667	1.9437
18	1.8028	2.0616
24	2.2361	2.4495

COM LL

H/V LL

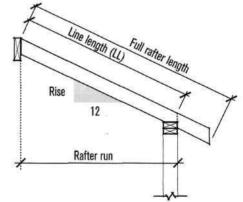
Roof

To convert Rafter Run to Line Length:

- 1) Select LL ratio for given slope in table above:
- 2) Multiply rafter run by LL ratio.

To find Full Rafter Length (add for any overhang at the eaves):

- Multiply the horizontal length of overhang by the same LL ratio;
- 2) Add this overhang length to the rafter LL.



When estimating rafter lengths and calculating spans, convert the rafter run (horizontal distance) to a sloped distance (line length) using these ratios.

Examples: On a 6/12 roof with a run* of 15 ft., find the net rafter length for the common rafters: 15 ft. x 1.118 = 16.77 ft. or 16 ft. 9½ in. Round up to the next 2-ft. increment for the lumber length needed (18-footers).

If the roof has a 16-in. overhang, measured along the rafter, the job will require 20-ft. rafters: 16 in. x 1.118 = 1.491 ft. + 16.77 ft. = 18.261 ft. or 18 ft. 3½ in. Round up to 20-footers.

^{*} For more precise calculations of rafters, use an effective run, which is shortened for the ridge thickness. For more information, see A Roof Cutter's Secrets to Framing the Custom Home (JLC Books)

Roofs

Estimating Rafter Length

To find the full rafter length, multiply the correct line length ratio in **Figure 3** by the horizontal run of the rafter. This gives the net rafter length, or line length, from top plate to ridge. Then add for the plumb cut at the ridge and overhang to find the full rafter length.

Estimating Number of Common Rafters

To calculate the number of common rafters, use the formulas provided in **Figure 2** (page 2) for the appropriate on-center spacing.

Remember to include ridge stock.

Estimating Hip and Valley Rafter Lengths

To calculate the length of each hip rafter, use the Hip/Valley LL ratio shown in Figure 3.

Estimating Jack Rafters

For a simple hip or valley, each pair of jack rafters is equal in length to one common (one long jack + one short jack = one common).

Estimating Roof Sheathing

ROOF AREA = PERIMETER WALL

LENGTHS (INCL. OVER HANCS)

x RAFTER LINE LENGTH

SHEATHING (4x8 PANELS) = ROOF AREA ÷ 32

- 1) Add overhang distance to exterior wall lengths;
- 2) Multiply the total length of the perimeter (wall length + overhang) by the rafter line length (**Figure 3**) to get total roof area (on gable roofs, don't include the gable-end wall in the total length);
- 3) Divide by 32 (for 4x8 panels).

Calculate roofs of different pitches individually.

Remember to add a couple of sheets to the total to account for error and waste.

Selecting Lumber

Selecting Dimensional Lumber

Dimensional lumber is differentiated by several species groups. The main species groups in the U.S. are SprucePine-Fir (Canadian), Douglas Fir-Larch, Hem-Fir, and Southern Pine (typically pressure-treated). Each species group is available in a number of grades, but unless otherwise

Figure 4. Strength of Wood

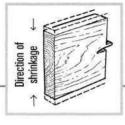
		Extreme Fiber Stress	Modulus of	
Species Group	Grade	in Bending (Fb)(2)	Elasticity (E)	
D-Fir-L	Select Strength	1,620	1.9	
	No. 1/ No. 2	1,020	1.6	
1 0	No.3	570	1.4	
SPF	Select Strength	1,500	1.5	
	No. 1/ No. 2	1,050	1.4	
	No. 3	600	1.2	
Hem-Fir	Select Strength	1,560	1.7	
	No. 1/ No. 2	1,200	1.6	
	No.3	690	1.4	
SYP	Select Strength	2,300	1.8	
	No. 1	1,500	1.7	
	No. 2	1,200	1.6	
	No. 3	600	1.4	

⁽¹⁾ These values include a size factor for 8-inch-wide nominal members used in normal conditions (lumber with a moisture content <= 19% placed on edge). Wet lumber or flat members require higher values. (2) psi (3) million psi

This table shows comparative design values for the four main wood species used in this manual. The values assume the lumber will be loaded on the edge. Extreme fiber stress in bending (Fb) is a measure of the lumber's strength to resist loads applied perpendicular to the grain. This load produces **tension** in the wood fibers along the edge farthest from the applied load, and **compression** in the fibers along the edge nearest to the load. The Modulus of Elasticity (E) is a ratio of the amount the wood will **deflect** in proportion to the applied load. **E is a measure of stiffness, whereas Fb is a measure of strength.**

Lumber Size	Actual Width	Width @ 19% MC (at Delivery)	Width @ 11% MC (Humid Climates)	Width @ 8% MC (Average Climates)	Width @ 6% MC (Arid Climates)
2x4	31/2"	31/2"	37/16"	33/8"	33/8"
2x6	51/2"	51/2"	53/8"	5 ⁵ /16"	55/16"
2x8	71/2"	71/4"	71/8"	71/16"	7"
2x10	91/4"	91/4"	91/16"	9"	8 ¹⁵ /16"
2x12	11 ¹ /4"	1 1 ¹ /4"	11"	1015/16"	107/8"

Figure 5. Predicted Shrinkage of Dimension Lumber



Framing lumber shrinks primarily across its width; shrinkage from end to end is insignificant. Actual shrinkage varies depending on the lumber's moisture content when delivered and the area's climate.

specified, most framing lumber is #2. Lower grades may be allowed for studs (Stud-Grade) and top plates (Utility-Grade).

Strength values for these and other North American species and species groups are shown in **Figure 4**. For convenience, the span tables in this book (pages 94-117) are listed by species group. If a species or group is not listed in the charts, use the spans for a species or group with the same or higher Fb value.

Shrinkage

Kiln-dried lumber is stamped K-D (kiln-dried) or S-Dry (surface dry), and is shipped with a moisture content

of about 19%. Anything larger than a 6x6 is generally not available K-D.

In a completed building, framing eventually dries to an average of 6% to 11% moisture content, depending on climate. This drying causes the lumber to shrink across the grain; shrinkage along the grain is negligible. Figure 5 shows the degree of shrinkage in flat-sawn framing lumber. Shrinkage in large carrying beams can cause one part of a house to settle more than others, causing drywall cracks and other problems (Figure 6).

However, using flush beams with hangers, or engineered lumber or steel, can reduce the potential for shrinkage problems. If dimensional

Figure 6. Avoiding Cumulative Shrinkage

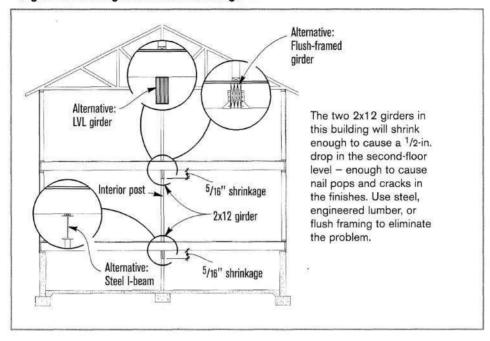
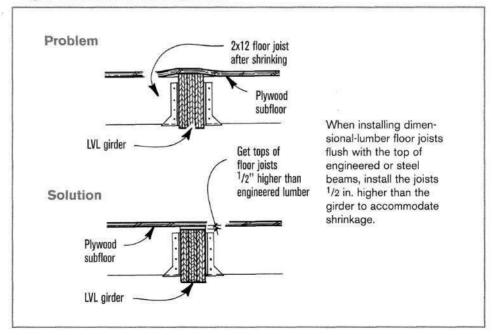


Figure 7. Flushed-Framed Floor Joists



The Essential Guide to Framing

lumber is hung flush from a beam made of steel or engineered lumber, the result can be a bulge at the beam (see Figure 7).

Selecting Sheathing and Subfloor Panels

Sheathing and subflooring should consist of performance-rated structural panels. These are made from plywood or oriented-strand board (OSB), and should carry a stamp (**Figure 8**) from APA-The Engineered Wood Association (formerly the American Plywood Association).

Panel Use Ratings

For framing, choose only from the following panel grades:

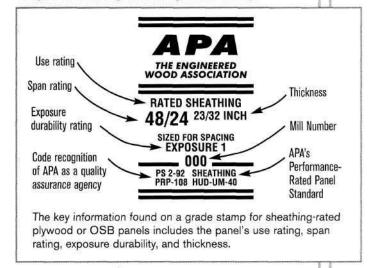
- Sheathing panels are designed for use on roof decks and walls;
- Structural 1 panels are designed for use on shear walls;
- Sturdi-Floor® tongue-and-groove panels are designed for use as subflooring.

Panel Exposure Ratings

For framing, select panels with only the following exposure ratings:

 Exterior panels can be used outdoors;

Figure 8. Reading Sheathing Grade Stamps



 Exposure 1 panels can withstand moisture during normal construction delays — up to a full season, according to APA. However, the panels should be covered up as soon as possible.

Other exposure ratings for wood panels include:

- Exposure 2 panels are typically used for protected construction and industrial applications where the potential for high humidity and water leakage may exist for limited times;
- Interior panels are made with water-soluble interior-grade glues and are intended for interior applications only, not for framing.

Panel Span Ratings

Span ratings on sheathing grade stamps may have two numbers such as 24/16. The first indicates the allowable roof span (in this case, 24 in. o.c.) and the second indicates the subflooring span (16 in. o.c.). Span ratings for multipurpose panels are: 24/0, 24/16, 32/16, 40/20, and 48/24.

If a sheathing panel stamp includes only one span number, the panel is for use on walls only.

Sturdi-Floor® panels are engineered for use as subflooring. They have span ratings of 16-, 20-, 24-, 32-, and 48-in.

Panel Thickness

Plywood and OSB are always $\frac{1}{32}$ in. smaller than their nominal sizes. For example, $\frac{1}{2}$ -in. plywood actually measures only $\frac{15}{32}$ in.

Roof Panel Span

Roof panels should be a minimum of 1/2 in. thick for 16-in. o.c. framing, and 5/8 in. thick for 24-in. o.c. framing.

For roofs framed 24-in. o.c., use H-clips to support the edges of the sheathing at mid-span. Clips create the proper gap and help stiffen panel edges.

OSB

While the strength and nail-holding ability of OSB and plywood are equal for similarly rated panels, OSB swells more when wet. Because of this, some builders avoid OSB in subflooring, especially in kitchens or baths, where exposure to wet conditions is likely. Some flooring contractors will not install hardwood flooring over OSB subflooring, although tests have shown that it performs the same as plywood in this application. OSB is not considered a suitable underlayment for use directly under ceramic tile or resilient flooring, however.

Unused OSB should be stored under cover on the job site. If an installed OSB subfloor is left uncovered for a long period after installation, consider treating it with a water repellent.

Selecting Engineered Lumber

Engineered studs and beams are not direct substitutes for solid lumber. Each engineered product has special installation requirements. Be sure to consult the product's technical literature before using any new engineered product.

Most engineered lumber is made with exterior glue. The glue will hold up under normal construction delays, but it is not waterproof. Therefore, all engineered lumber should be protected from the weather on-site and stored flat.

Wood I-Joists

Using wood I-joists places the strongest material (typically LVL) where the bending stresses are greatest — in the *flanges* along the top and bottom of the beam. This lets the lightweight beams span great distances with minimal deflection, providing a very stiff floor.

I-joist webs consist of plywood or OSB, making them more susceptible to water damage than sawn lumber. Therefore, I-joists must be stored under cover — particularly those with OSB webs. Care must be taken when drilling or notching the webs to allow mechanicals to pass through (see "Boring and Notching I-Joists," page 31).

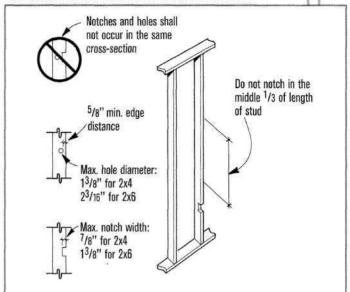
Engineered Studs

For tall walls and kitchen walls that must remain straight for countertop and cabinet runs, engineered studs are a cost-effective alternative to dimensional lumber. Follow manufacturers' guidelines for installing specific products. General use precautions are shown in **Figure 9**.

Finger-jointed studs aren't any stronger than dimensional lumber of the same species, but because the defects have been cut out, they are more dimensionally stable. In addition, the grain is interrupted by glue joints, making finger-jointed studs less likely to twist and bow.

The glue that holds the joints together is water-resistant, but these studs should be protected from prolonged exposure to the weather.

Figure 9. Engineering Studs for Tall Walls



Certain restrictions may apply to drilling holes and cutting notches in tall engineered studs. Whenever using engineered lumber, consult the manufacturer's specs for design values, load tables, and nailing requirements.

Laminated Strand Lumber (LSL).

LSL is made from strands of wood bonded with a polyurethane adhesive, and it is used mostly for rim boards, studs, and headers. LSL studs are straight and true, but heavier than solid lumber. They have sharp edges so wear gloves when handling. LSL studs take air nails about the same way dimensional lumber does, but there are fewer problems with splits if nails are kept at least ½ in. from the edges.

Engineered Beams

Engineered beams may consist of laminated veneer lumber (LVL),

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glue-laminated timbers (glulams), or parallel-strand lumber (Parallam®). Be aware that the large loads carried by an engineered beam will concentrate at the bearing points. To keep the beam's fibers from crushing under the weight, be sure to allow sufficient bearing surface. Installation of large engineered beams may require a crane or lift.

Laminated-Veneer Lumber (LVL). LVL is a strong, versatile, engineered product that resembles plywood. LVL beams are typically built up from several LVL members nailed or bolted together. Bolting is preferable where the beam is side-loaded (e.g., a floor system with flush framing) or where it will be exposed to the weather. Side loading with joist hangers can cause the outer LVL members to "peel off" if they are not bolted together.

Before ordering LVL, it's important to note the grade, species, and manufacturer specified by the designer. For example, Douglas-fir LVL is somewhat weaker than yellow-pine LVL. While most LVL has a water-resistant coating, it is still vulnerable to cupping when exposed to moisture. So store it dry.

Glue-Laminated Timbers (glulams). A glulam consists of dimension lumber face-laminated with structural adhesives. Three appearance grades are available — industrial, architectural, and premium. Design values are the same for all three

grades, but the better grades have fewer surface defects. This is important in residential construction where most glulams are left exposed.

Glulams come in widths ranging from $2^{1}/2$ to $10^{3}/4$ in. Depths are multiples of the lamination thickness. For example, a glulam with eight $1^{1}/2$ -in. laminations will be 12 in. deep.

Most glulams are delivered in a wrapping that protects the surface of any exposed beam during shipping and installation. If possible, don't remove this wrapping until all interior finishing is complete. Protect wrapping so that water doesn't leak in and become trapped.

Never notch or drill a glulam without consulting either the fabricator or a structural engineer. Connections should be made so that the beam can swell and shrink with moisture swings.

Parallel-Strand Lumber (Parallam®). Sold under the brand name Parallam®, this product consists of strands of veneer that are aligned, coated with glue, and cured with a combination of pressure and microwaves. The resulting beam is stronger and stiffer than solid-sawn lumber and is equivalent in strength to multiple LVLs. However, you save the expense of bolting and don't need to worry about side loading or warping from moisture. The material is somewhat harder to cut and nail than solid lumber.

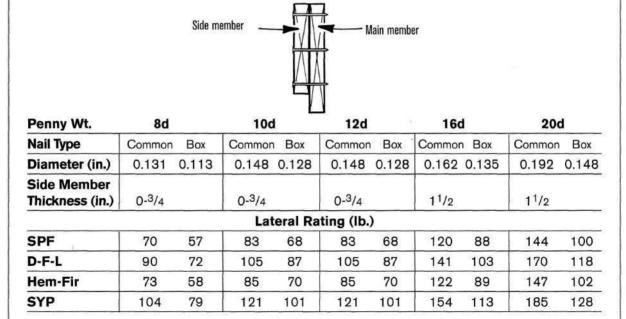
Nails

Holding Power of Nails

A nail's holding power is a function of its diameter, how far it penetrates the wood, and the type of wood it penetrates. In framing, nails should never be loaded in withdrawal (where the load acts parallel to the nail shank and tries to pull it out). Instead, framing

nails should be loaded only laterally (where the load acts perpendicular to the shank). Also, nails have more holding power when driven into the side grain rather than into the end grain. In fact, nailing into the end grain will reduce a nail's lateral load capacity by approximately one-third.

Figure 10. Lateral Strength of Common vs. Box Nails



Nails are rated for "lateral capacity," which is greatly affected by the nail's diameter. Since box nails are skinnier than commons, they have lower strength values. The values shown vary with the type of framing lumber used, and they assume the nail will penetrate the main member (illustration at top) at least 12 diameters.

Box vs. Common Nails

Lateral strength is largely a function of a nail's diameter and the density of the type of wood into which the nail is driven. For example, 10d and 12d nails have the same diameter and the same lateral strength in each type of wood.

Figure 11. Conversion Ratio for Common to Box Nails

To convert required number of common nails of a given size to box nails, multiply by the appropriate ratio and round up.

Penny Wt.	8d	10d	12d	16d	20d	
Ratio	1.23	1.22	1.22	1.36	1.44	

S-P-F lumber assumed.

Do not substitute a common nail that's specified on the plans for an equal number of box nails. Instead, multiply the specified number of common nails by the conversion ratio shown in the chart and round up to find the equivalent number of box nails. Common nails are stronger than box nails because of their greater diameter (Figure 10).

When substituting box for common nails, calculate the nail size needed using the conversion ratios shown in Figure 11.

Withdrawal Strength of Nails

Nails are much stronger when loaded laterally (across the nail) than when loaded in withdrawal (along the length of the nail). Withdrawal from end grain is particularly weak and not accepted as a structural connection by most codes. Withdrawal values from sidegrain are given in Figure 12.

Figure 12. Withdrawal Strength Design Values of Common vs. Box Nails

Penny Wt.	8d		10d	l	12d		160	d	200	d
Nail Type	Commor	Вох	Common	Вох	Common	Вох	Commo	n Box	Common	Вох
Diameter (in.)	0.131	0.113	0.148	0.128	0.148	0.128	0.162	0.135	0.192	0.148
			Wi	thdraw	al Value	*				
SPF	21	18	23	20	23	20	26	21	30	23
D-F-L	32	28	36	31	36	31	40	33	47	36
Hem-Fir	22	19	25	21	25	21	27	23	32	25
SYP	41	35	46	40	46	40	50	42	59	46

^{*} psi per inch of penetration into side grain of main member

This table shows the allowable load values for typical common and box nails. These values represent the pounds per square inch of load applied per penetration into the side grain of the main member.

Toenails

For toenails loaded in withdrawal, multiply the values in Figure 12 by .67. For toenails loaded laterally, multiply the values in Figure 10 by .83. Toenails should be driven at an angle of about 30 degrees from the face of the stud or other member being attached (Figure 13).

Pneumatic Nails

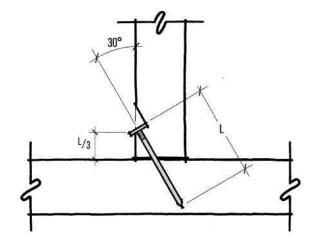
Pneumatic nails are typically sold by a specified shank diameter in inches (.120, .131, and .148 are common for framing nails). These are typically skinnier than common nails of equal length and, therefore, have lower lateral strength (**Figure 14**) and withdrawal values (**Figure 15**). Consult manufacturers for lateral strength of specific nail types.

Galvanized Nails

Galvanized nails are made from zinccoated steel. The zinc protects the steel from rust. How well a nail resists rust depends on the amount of zinc and how it's applied.

Hot-dipped nails (coated by immersion in molten zinc) are the most durable.

Figure 13. Proper Toenailing



Place toenails away from the end of the board a distance that's equal to one-third the length of the nail. Angle the nail so it comes through at the center of the board's thickness.

Figure 14. Lateral Strength of Air Nails

	Wood Species					
Nail Diameter	SPF	DFL	Hem-Fir	SYP		
0.12"	19	29	20	37		
0.131"	21	32	22	41		
0.148"	23	36	25	46		
0.162"	26	40	27	50		

Values are based on a 10-year "normal" load duration, and assume: 1) smooth-shank nails driven perpendicular to the wood grain; and 2) both side and main members are of the same wood species. When toenailing, multiply the values by .83, as described in "Toenails," top of page.

Figure 15. Withdrawal Strength Load Values for Air Nails

		Wood Species				
Nail Length	Nail Dia.	SPF	DFL	Hem-Fir	SYP	
21/2"	0.131"	52	62	54	67	
3"	0.12"	69	81	71	89	
3"	0.131"	79	93	80	101	
3"	0.148"	84	99	86	109	
31/4"	0.12"	69	81	71	89	
31/4"	0.131"	79	93	80	101	
31/2"	0.162"	92	109	94	119	

Withdrawal values (psi per inch of penetration into the main member) are based on a 10-year "normal" load duration, and assume: 1) smooth-shank nails driven perpendicular to the wood grain; and 2) both side and main members are of the same wood species. When toenailing, multiply the values by .83, as described in "Toenails," previous page.

Hot-galvanized (HG) nails are coated with zinc chips in a hot tumbler, a process that can leave an uneven coating. A certain percentage of these nails will rust when used outside.

Electroplated nails are smooth and shiny, but the thin zinc coating will oxidize away quickly when exposed. This makes them a poor choice for exterior work.

Mechanical plated, or "peen" plated, nails have a zinc layer that isn't as thick as that used on a hot-dipped nail, so it is less corrosion-resistant. However, mechanical plating is appropriate for screws as the thin coating won't clog the threads.

Figure 16. Nailing Schedules

Roof Framing	Number of Common Na	ails Number of Air Nails
Rafter to top plate (toe-nailed)(1)	3-8d per rafter	3-3 x .131 per rafter
Ceiling joist to top plate (toe-nailed)(1)	3-16d per joist	5-3 x .131 per rafter
Ceiling joist to parallel rafter (face-nailed)(1)(2)	3-16d per joist	4-3 x .131(1) per rafter
Ceiling joist laps over partitions (faced-nailed)	3-16d per lap	4-3 x .131 per rafter
Collar tie to rafter (face-nailed)(1)	3-16d per joist(1)(2)	4-3 x .131 per rafter
Blocking to rafter (toe-nailed)	2-8d each end	2-3 x .131 each end
Roof rafter to ridge beam ⁽¹⁾	3-10d per rafter	3-3 x .131 per rafter
Jack rafter to hip (toe-nailed)	3-10d per rafter	3-3 x .131 per rafter
Roof Sheathing(1)		
Structural panels	1-8d every 6 in. edge, 12 in. field	1-2 ¹ / ₂ x .131 every 6 in. edge, 12 in. field

Figure 16. Nailing Schedules, continued

Wall Framing	Number of Common Nails	Number of Air Nails		
Top or bottom plate to stud (end-nailed)(1)	2-16d per stud	3-3 x .131 per stud		
	3-16d per 2x6 stud	4-3 x .131 per stud		
Top or bottom plate to stud (toe-nailed)(1)	3-16d per stud	4-3 x .131 per stud		
	4-16d per 2x6 stud			
	5-16d per stud	3-3 x .131 per stud		
Top plate to top plate (face-nailed)(1)	2-16d every 16 in.	2-3 x .131 every 12 in.		
Top plates at intersections (face-nailed)	2-16d each side of joint	4-3 x .131 each side of join		
Stud to stud (face-nailed)	2-16d every 24 in.	2-3 x .131 every 16 in.		
Header to header (face-nailed)	1-16d every 16 in. along edges	1-3 x .131 every 12 in. along edges		
Bottom plate to floor joist, band joist, end joist, or blocking (face-nailed)(3)(4)	1-16d every 16 in.	1-3 x .131 every 8 in. along edges		
Wall Sheathing ⁽¹⁾				
Structural panels	1-8d every 6 in. edge, 12 in. field	1-2 ¹ / ₂ x .131 every 6 in. edge, 12 in. field		
Floor Framing				
Joist to sill, top plate or girder (toe-nailed)	4-8d per joist	4-3 x .131 per joist		
Bridging to joist (toe-nailed)	2-8d each end	2-21/2 x .131 each end		
Blocking to joist (toe-nailed)	2-8d each end	2-21/2 x .131 each end		
Blocking to sill or top plate (toe-nailed)	3-16d each block	4-3 x .131 each block		
Ledger strip to beam (face-nailed)	3-16d below each joist	4-3 x .131 below each jois		
Joist on ledger to beam (toe-nailed)	3-8d per joist	3-3 x .131 per joist		
Rim joist to joist (end-nailed)	3-16d per joist	4-3 x .131 per joist		
Rim joist to sill or top plate (toe-nailed)(1)	2-16d every 12 in.	2-3 x .131 every 8 in.		
Floor Sheathing				
Structural panels				
1 in. or less	1-8d every 6 in. edge, 12 in. field	1-2 ¹ / ₂ x .131 every 6 in. edge, 12 in. field		
Greater than 1 in.	1-10d every 6 in. edge,	1-3 ¹ / ₄ x .131 every		

⁽¹⁾ For high wind areas, consult local codes.

⁽²⁾ See Figure 87, page 53, for detailed schedules to accommodate specific roof loading conditions.

⁽³⁾ Nailing requirements are based on wall sheathing nailed 6 in. o.c. at the panel edge. If wall sheathing is nailed 3 in. o.c. at the panel edge to obtain higher shear capacities, nailing requirements for structural members must be doubled, or alternate connectors, such as shear plates, must be used to maintain the load path.

⁽⁴⁾ When wall sheathing is continuous over connected members, the tabulated number of nails can be reduced to 1-16d nail per foot.

Aluminum and Stainless-Steel Nails

Aluminum nails are sometimes used to fasten exterior siding. They're very resistant to rust and corrosion, but may corrode when used with some flashing metals.

Stainless steel. While expensive, stainless-steel nails are the most rust-resistant under nearly all conditions. They are highly recommended below grade or in homes that will be exposed to salt air. They're also recommended for cedar or redwood trim, and for siding that will be left to weather without stain or paint. Stainless-steel nails are typically available as Type 304 and 316. Type 316 are more durable.

Nailing Rules of Thumb

Typical nailing schedules appear in Figure 16.

Two is better than one. In general, never rely on a single nail. Use at least two.

Nail spacing. Don't space nails closer than one-quarter their length to the edge of the board.

Nail penetration. To hold at full strength, nails should penetrate the wood a depth that's at least 11 times their diameter — $1^{1/2}$ in. for 8d nails and $1^{3/4}$ in. for 16d nails.

Framing Connectors

Hangers for Solid Wood Joists

When using joist hangers, it's critical that you use the proper size hanger and fill all holes with nails.

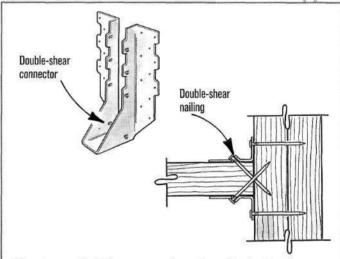
Do not split ends. A nail that splits the wood will reduce the joist's carrying capacity. In critical situations, you can predrill nail holes a depth of up to three-quarters the nail's diameter.

Double-shear connectors provide greater strength with fewer nails (**Figure 17**).

Joist-Hanger Nails

A particular hanger may call for 8d, 10d, 12d, or 16d common nails. Special joist-hanger nails also may be used. Though they have 8d or 10d shank diameters, they are only 1½-t to 1½-in. long, so they can be driven into the joist without protruding through the other side. Using them where the hanger calls for full-length 10d or 12d nails will reduce the hanger's load capacity by 20% to 30%. Hanger catalogs give adjustment factors for specific nail sizes. Don't use joist-hanger nails in place of longer nails

Figure 17. Double Shear Connectors



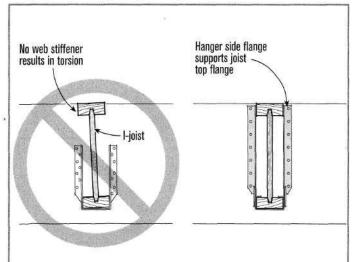
The strongest joist hangers are those that offer double shear nailing that crosses the joist ends. The angle also makes it easier to nail them to the joist in a joist bay.

in double-shear hangers or as face nails on skewed hangers.

Effect of Lumber Shrinkage on Hangers

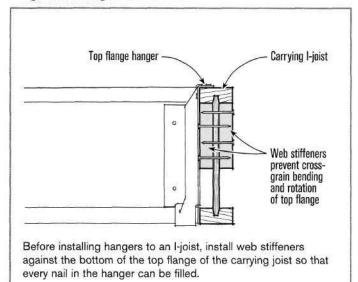
Joist hangers are designed for use with dry lumber. If lumber is wet, shrinkage may leave a gap between the bottom of the joist and the hanger's saddle or between the top of the joist and the floor decking.

Figure 18. I-Joist Hanger Height



The strongest joist hangers are those that offer double shear nailing that crosses the joist ends. The angle also makes it easier to nail them to the joist in a joist bay.

Figure 19. Hangers on I-Joists



Wood I-Joist Hangers

Wood I-joists require special hangers. Do not try to adapt conventional hangers.

I-Joist Hanger Height

Hangers for wood I-joists should be tall enough to catch the I-joist's top flange unless a web stiffener is used; otherwise, the joist may roll in the hanger (**Figure 18**). If a web stiffener is used, the hanger side flange should be at least 60% of the joist depth.

I-Joist Hanger Width

Hangers for wood I-joists should be the same width as the joist flange. Do not trim the flange to fit a narrower hanger; this would reduce the joist's strength. A wider hanger will either leave a gap, potentially causing a squeak, or will require filling with plywood, which would unevenly load the hanger.

Nailing I-Joist Hangers

Nail in every hole with correct sized nails; leaving nails out greatly reduces the hanger's capacity. Nails that are too long can hit the bottom of the hanger and curl under the joist, causing a squeak.

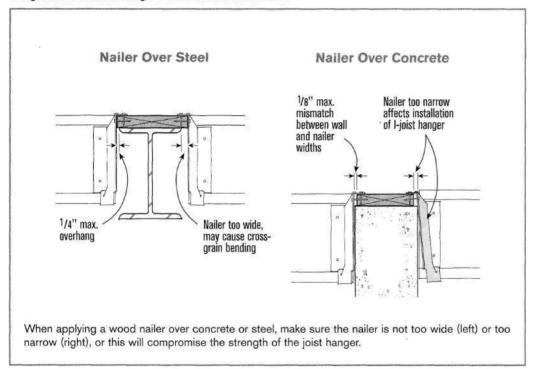
Web Stiffeners

For I-joist to I-joist connections, install web stiffeners against the bottom of the top flange of the carrying joist (**Figure 19**).

Wood Nailers for I-Joists

For hangers that bear on wood nailers, the nailer should not overhang its support more than 1/4 in. or sit more than 1/8 in. in from the edge (**Figure 20**).

Figure 20. I-Joist Hangers on Concrete and Steel



Floors: DIMENSIONAL LUMBER

Floor systems get their strength from the diaphragm action of the subflooring, which is typically T&G plywood glued and either nailed or screwed over uniformly spaced joists.

Joist Depth

Rule of thumb. Most codes assume residential floor loads to be 50 pounds per sq. ft. — 40 pounds live load plus 10 pounds dead load. If load conditions do not exceed this value, you can use the following rule of thumb for sizing uniformly loaded residential floor joists:

Figure 21. Live Loads for Floors and Ceilings

Component L	ive Load (lbs./sq. ft.)
Residential rooms	40
Decks	60
Balconies	60
Fire escapes	40
Stairs	40
Ceiling joists (limited attic stor	rage) 20
Ceiling joists (no attic storage) 10

Live loads include all loads that are not part of the building itself (dead loads), such as people, furnishings, wind, and snow.

HALF THE SPAN + 2 = IOIST DEPTH

First, round the clear span of the floor joist up to the nearest foot and divide by 2. Then add 2 to the answer. For example: For a clear span of 15 ft. 6 in., round up to 16 and divide this span by 2, giving you 8. Next, add 2 to get the required depth in inches (8 + 2 = 10). It's important to use the *actual* lumber dimensions, not the nominal dimensions, so a 2x12 floor joist will be required.

Design Loads for Floor Joists

Live loads. A 40-psf live load will meet most codes for residential living spaces (some require only 30 psf in bedrooms). For typical live loads, see Figure 21.

Dead loads. For dead loads, 10 psf is adequate for standard wood-frame construction. For mortar-set ceramic tile floors, frame for a 20-psf dead load. For other special situations, calculate loads based on weights of building materials (Figure 22).

Figure 22. Weights of Common Building Materials

Materials	Pounds per Sq. Ft.	Materials	Pounds per Sq. Ft.
Studs, Joists & Raf	ters	Flooring	
2x4s, 16 in. o.c.	9	3/4 in. hardwood strip flo	oring 4
2x6s, 16 in. o.c.	1.4	3/8 in. ceramic tile	2.5
2x6s, 24 in. o.c.	1	1/2 in. quarry tile	6
2x8s, 16 in. o.c.	1.9	1 in. mortar bed	12
2x8s, 24 in. o.c.	1.3	Cement backerboard	3.5
2x10s, 16 in. o.c.	2.4	Carpet and pad	3
2x10s, 24 in. o.c.	1.6	Exterior Wall Cladding	1
2x12s, 16 in. o.c.	2.9	Wood siding	1.5
2x12s, 24 in. o.c.	2	Three-coat stucco	10
Residential roof truss	s, 24 in. o.c. 4	Window unit	8
Sheet Goods		Roofing	
¹ /2 in. plywood	1.5	Asphalt shingles	2.5 - 4.5
³ /4 in. plywood	2.3	Clay tiles	9 - 12
¹ /2 in. drywall	2	Spanish tile	19
⁵ /8 in. drywall	2.5	Mortar bed for roof tile	10
	s an approximate guide for for the exact weight of specific	Insulation (per in. thic	kness)
	eck with the manufacturer.	Fiberglass batt insulation	.05
		Rigid foam	.2

Joist Spacing

Floor and ceiling joists are usually framed 16 in. o.c. However they may be framed at 12 in. o.c. to increase stiffness, or to increase the span in one section of a floor system without changing lumber depth.

Joist Span Tables

Joist span means the clear, horizontal distance between supports (**Figure 23**). The actual joist length is longer to provide bearing at each end (see "I-Joist Bearing," page 31). Spans for dimensional lumber floor and ceiling joists are given in **Figures 24 to 27**, pages 94-97.

If the species or species group you are using is not listed, choose one with the same or slightly lower Fb values in **Figure 4**, page 6. If necessary, you can interpolate between two values.

Figure 23. Joist Span

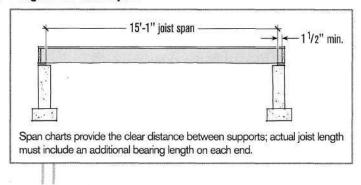
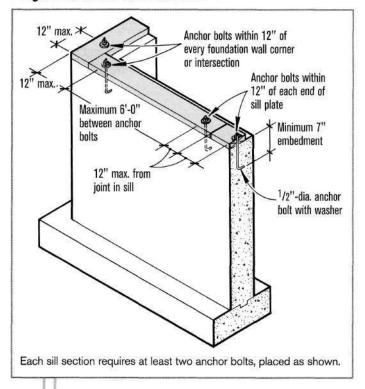


Figure 28. Anchor Bolt Placement



Framing Details

Sill Plates

For sill plates in contact with concrete or masonry foundations, use pressuretreated wood to protect against decay and insect attack.

Anchor Bolts

Bolt the sill plate to the foundation with anchor bolts or strap anchors spaced no more than 6 ft. apart.

Most codes call for minimum ¹/₂-in. steel J-bolts embedded at least 7 in. in concrete, mortar joints, or solid-grouted masonry units. Each section of sill must have at least two bolts, with one bolt placed somewhere between 3¹/₂ to 12 in. from each end (**Figure 28**). Each bolt needs a nut and adequately sized washer.

Wedge anchors. If anchor bolts are missing, use 1/2-in. wedge anchors or adhesive anchors that use hammer-in glass capsules. With a wedge anchor, tightening the nut expands the anchor until it's locked tight against the sides of the hole. A wedge anchor must be tightened to the manufacturer's specified torque. Tightening it too much can pulverize the surrounding concrete. Also, anchors can't be placed too

close to the edge of a concrete slab or foundation wall.

Adhesive anchors. Adhesive anchors can be spaced closer to each other, and closer to the edge of a slab or wall, than wedge anchors. Drill a hole in the concrete and drop the capsule in. Then pound the anchor into the hole with a small sledgehammer; this mixes the chemicals in the capsule. Note: The capsules have a long shelf life, but should be protected from freezing.

Joist Bearing

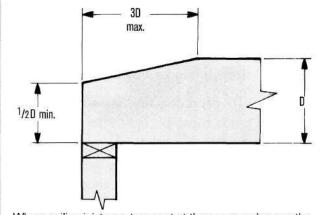
Joists should have at least $1^{1}/2$ in. of good bearing on wood or metal, or 3 in. on masonry (**Figure 23**). If necessary, you can safely notch a joist at its bearing point up to one-sixth the depth of the joist.

Ceiling joists are often tapered to fit beneath the roof rafters. But tapering them too much will weaken the joists at their bearing point. If you must taper the ends of a ceiling joist, follow the guideline shown in **Figure 29**.

Boring and Notching Joists

In general, do not make any notches in the middle third of a joist. Also, avoid vertical cuts in the bottom of a joist; angle the cuts instead to reduce the likelihood of splitting. For other rules, follow the recommendations in **Figure 30**.

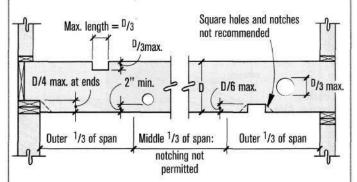
Figure 29. Tapered Joist Ends



Where ceiling joists are taper-cut at the eaves, make sure the width of the cut does not exceed three times the joist depth and that the end of the joist is at least half the depth.

Figure 30. Cutting, Notching, and Boring Lumber Joists

Joist Size	Maximum Hole	Maximum Notch Depth	Maximum End Notch
2x4	None	None	None
2x6	11/2	7/8	13/8
2x8	23/8	11/4	17/8
2x10	3	11/2	23/8
2x12	33/4	1 ⁷ /8	27/8



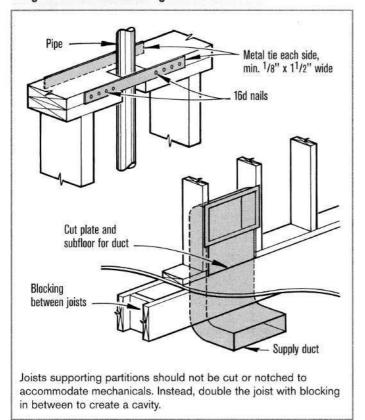
Do not notch a span's middle third where bending forces are greatest. For all calculations, use actual, not nominal, dimensions.

Where mechanicals need to pass through a joist supporting a partition, double the joist with blocking in between to create a cavity (**Figure 31**).

Rim Joists and Bridging

To prevent joists from twisting, the ends must be nailed to a solid band joist (rim joist) or header. If there is no band joist or header, nail solid blocking between the joist ends. Most codes don't require additional bridging

Figure 31. Accommodating Mechanicals



unless the joist is at least six times as high as it is wide, in which case bridging is needed every 8 ft. However, solid or X-type bridging at mid-span will help stiffen any floor.

Load Paths

All loads start at the roof and must transfer on an unbroken path through structural elements to the foundation. Many cracking problems, which are misinterpreted as "settling," are actually caused by broken load paths. These broken paths result in loads being carried by areas that were not designed to carry them.

Support for Loadbearing Walls

Parallel to joists. Ideally, if a loadbearing wall runs parallel to the floor joists, then it should sit directly over a beam or a joist supported by a loadbearing wall below. If the loadbearing wall sits between two joists, complete the load path by installing solid blocking between the two joists every 16 in. o.c.

Perpendicular to joists. If a loadbearing wall runs perpendicular to the floor joists, it should be offset from a supporting beam or loadbearing wall below by no more than the depth of the joists (Figure 32).

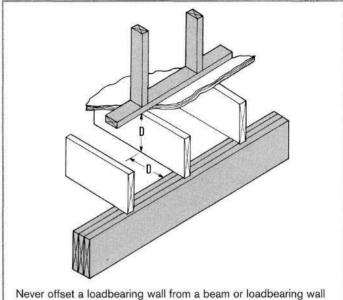
Support for Non-Loadbearing Walls

A non-loadbearing wall that runs parallel to the joists doesn't need to be placed directly over a joist. However, when it's not directly over a joist, solid blocking should be installed between the joists to carry the load (Figure 33). If the wall is placed directly over a joist, that joist should be doubled.

Point Loads

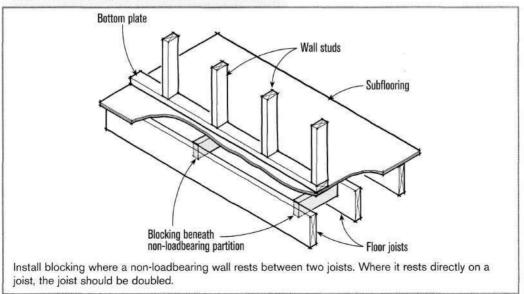
A concentrated load that bears on a floor system — such as a structural post must sit directly over a post or beam below. In addition, solid blocking (with a cross-section at least as large as the post) must carry the load through the floor system to the underlying post or beam.

Figure 32. Aligning Bearing Walls



below by more than the depth of the joists.

Figure 33. Blocking under Non-Loadbearing Walls

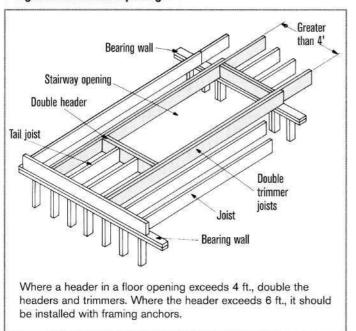


Floor Openings

Where a floor opening is more than 4 ft. wide, both the headers and trimmers should be doubled (Figure 34). Headers over 6 ft. long must be fastened with steel connectors and should be sized according to the load.

A tail joist in a framed opening that's over 12 ft. long should be connected with hangers. Otherwise, it should sit on a 2x2 (min.) ledger nailed to the face of the header.

Figure 34. Framed Openings



Cantilevered Floors

Basic framing details for all cantilevers are shown in **Figure 35**.

Loadbearing Cantilevers

Where a cantilevered floor supports only a roof load with a total span of 28 ft. or less (such as on a Garrison-style home), the joists may cantilever up to one-eighth the length of the lumber span. Where the loads are greater, the cantilever should not exceed the depth of the joists unless the system is engineered.

Non-Loadbearing Cantilevers

A cantilever that supports a non-loadbearing wall should not exceed onefourth the joist span. For non-loadbearing cantilevered decks (floor load only), the maximum overhang is onethird the span (**Figure 36**).

Engineered Cantilevers

Cantilevers that exceed these limits should be engineered. Doubling joists or reducing joist spaces, along with upgrading connections, often permits greater overhangs.

Figure 35. Cantilever Details

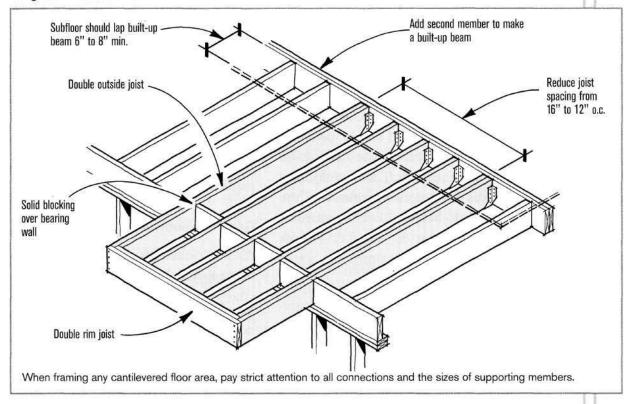
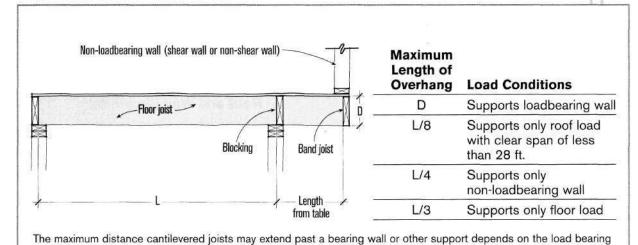


Figure 36. Cantilever Rules of Thumb

on the end of the cantilever.



Floors: SUBFLOORING

The best quality subfloor consists of tongue-and-groove (T&G) plywood that's glued and either nailed or screwed to the joists. T&G subflooring improves the perceived stiffness of the floor, and helps prevent squeaks. Subflooring that is not T&G must have solid blocking under all joints between panels.

Subfloor Spans

While T&G subflooring does not require solid blocking at joints, every sheet must rest on at least two joists. Panels are rated for spans of 16-, 20-, or 24-in., depending on thickness and grade. Span information is stamped on individual sheets (**Figure 8**, page 9).

Fastening Subfloor Panels

Nail panels with minimum 6d common nails, spaced 6 in. o.c. at the edges of the panel and 12 in. o.c. in the field. Keep nails at least $\frac{3}{8}$ in. from

edges. (For shear wall nailing requirements, see "Shear Walls," page 74.)

For nailing schedules, see **Figure 16**, pages 16-17.

Gaps for Subfloor

APA recommends that subfloor panels be gapped ½8 in. along the ends and edges. A 10d box nail may be used to gauge the spacing.

Gluing Subfloor

When nailing subfloor panels to joists under wet conditions, use a construction adhesive labeled AFG-01 and/or ASTM D 3498. Solvent-based construction adhesives typically dissipate the water better than latex- and ure-thane-based adhesives.

Roof and Wall Sheathing

Do not glue roof or wall sheathing to framing. Sheathing panels tend to be thinner than subflooring panels, so they're more likely to buckle when wet.

Floors: WOOD 1-JOISTS

Spans, installation details, and other wood I-joist specifications vary from one manufacturer to the next. Therefore, it is important to consult the manufacturer's literature when using these products.

Boring and Notching I-Joists

Rules vary, depending on the I-joist manufacturer, but the following guidelines generally apply to cutting holes in wood I-joists.

No Holes Through Flanges

Never make holes or saw cuts in I-joist flanges — the bending stresses are too high. Even a shallow kerf in the lower flange can critically weaken an I-joist.

Holes in Webs

Follow manufacturers' guidelines for minimum distances between holes and the bearing point (**Figure 37**). Use manufacturers' knockouts where practical. In general, you can cut a hole up to $1^{1}/2$ in. in diameter anywhere in the web.

Hole size. Permissible hole size increases as you near the center of the span where shear stresses are the smallest. Most manufacturers require that the distance between two holes be at least twice the diameter of the larger hole.

Avoid rectangular cutouts. With rectangular holes in webs, avoid overcutting the corners. Rounded corners are best. One technique is to drill a 1-in. hole in each corner and then cut between the holes.

I-Joist Bearing

Most I-joists require at least 1³/₄ in. of bearing at each end. If the end of the joist is cut at a bevel, the top chord must also extend beyond the face of the wall (**Figure 38**).

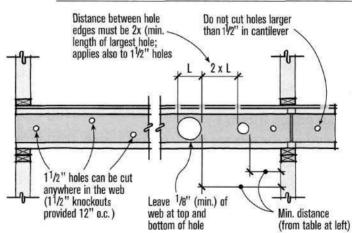
Temporary Bracing for I-Joists

Unbraced I-joists are flimsy and unstable until they are fully braced and sheathed. It doesn't take much to roll them over and damage them, so install

Figure 37. Cutting and Notching Rules for Wood I-Joists

Min. Distance (ft.-in.) from Inside Face of Support to Near Edge of Hole

I-Joist Depth	TJI/Pro		Ho	le Diame	eter	
91/2"	150	1'-0"	1'-6"	3'-0"	5'-0"	6'-6"
	250	1'-0"	2'-6"	4'-0"	5'-6"	7'-6"
117/8"	150	1'-0"	1'-0"	1'-0"	2'-0"	3'-0"
	250	1'-0"	1'-0"	2'-0"	3'-0"	4'-6"
	350	1'-0"	2'-0"	3'-0"	4'-6"	5'-6"
	550	1'-0"	1'-6"	3'-0"	4'-6"	6'-0"
14"	250	1'-0"	1'-0"	1'-0"	1'-0"	1'-6"
	350	1'-0"	1'-0"	1'-0"	1'-6"	3'-0"
	550	1'-0"	1'-0"	1'-0"	2'-6"	4'-0"
_3	250	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"
	350	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"
	550	1'-0"	1'-0"	1'-0"	1'-0"	2'-0"



Note: Distances in the charts above are based on uniformly loaded joists using the maximum loads shown in Trus Joist's brochure. For other load conditions or hole configurations, contact a Trus Joist representative. For simple span (5-foot minimum) uniformly loaded joists, one maximum-size hole may be located at the center of the joist span provided no other holes occur in the joist. DO NOT cut into joist flanges when cutting out web.

Most manufacturers allow holes up to 11/2 in. anywhere in the web, but require that the distance between any two holes be at least twice the diameter of the larger hole. In all cases, follow manufacturer's specifications for hole locations. The example provided here is courtesy of Trus Joist. Larger holes are allowed per manufacturer's specification.

all blocking and rim boards as soon as possible.

Sheathing and 1x4 Bracing

Stabilize the joists by sheathing the first 4 ft. of the floor system at one end of the joist bays and then bracing the rest of the joists to the sheathing area with 1x4 braces placed every 6 to 8 ft. Nail the braces flat to the top of the joists and lap them at the ends by at least two joists.

Avoid Overloading I-Joists

Be careful not to overload I-joists with heavy construction materials, such as stacks of plywood or pallets of bricks. If such loads are unavoidable, place them directly over loadbearing walls, posts, or other suitable supports.

I-Joist Load Paths

Loadbearing walls should be stacked over girders or loadbearing walls below. Use squash blocks or I-joist blocking to carry the load through the floor system (Figure 39).

Do not offset loadbearing walls unless the design has been engineered.

Figure 38. I-Joist Bearing

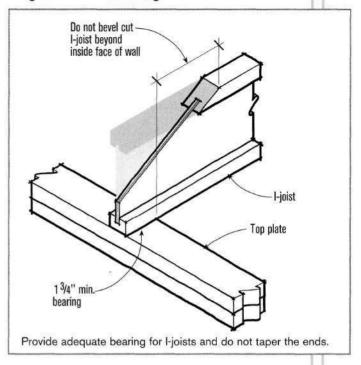
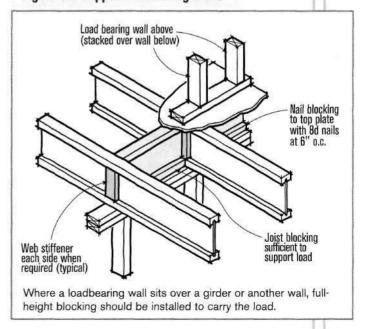
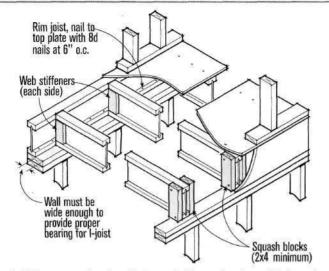


Figure 39. Support for Bearing Walls



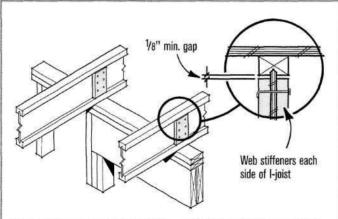
The Essential Guide to Framing

Figure 40. Rim Joists



In I-joist construction, band joists typically consist of wood I-joists, plywood, or special composite rim joist materials. Web stiffeners may be required on long spans. Squash blocks may be required with thinner rim joist materials when there is a loadbearing wall above. Check manufacturer's specifications.

Figure 41. Web Stiffeners



Web stiffeners of plywood, OSB, or 2x lumber (for large I-joists) are required at certain bearing points to transfer shear and prevent buckling of the web. Except where there is a concentrated load from above, web stiffeners should fit tight to the bottom flange with a space at the top. Web stiffeners also provide solid nailing at joist hangers. Follow manufacturers' nailing schedules.

Rim Joists for I-Joist Floors

To keep joists from twisting — and to help transfer loads from the wall above to the wall or foundation below — either attach the ends of I-joists to a full-height (band) joist or header or install blocking between the joists.

Rim Joist Materials

Acceptable rim joist materials include: the same-size I-joists as those used in the floor system; one or two layers of plywood or OSB; or an engineered lumber or metal product (**Figure 40**).

Don't mix wood I-joists with solid lumber rim joists. Not only are the two materials difficult to match in height, but also solid lumber will shrink after installation, leaving too much weight on the I-joists.

Web Stiffeners for I-Joists

Web stiffeners of plywood, OSB, or 2x are used to keep I-joist webs from buckling at bearing points or other intersections. (Thin web materials cannot transfer large shear forces.) With joist hangers, web stiffeners are often required to provide solid nailing.

Web stiffeners at bearing points should be installed tight to the top of the bottom flange. Leave a ½-to ½-in. space at the top flange to prevent the stiffener from prying the top flange off under load (**Figure 41**). One exception is

where the joists support a load from above at mid-span. In this case, install the stiffener tight to the top flange with the space at the bottom.

Web stiffeners go on both sides of an I-joist with the face grain parallel to the length of the joist (for plywood and OSB stiffeners). Nail plywood or OSB stiffeners from each side with three or more 8d nails, staggered and clinched at the ends. For solid 2x stiffeners, use three 16d nails (two from one side, one from the other) and clinch the ends if they penetrate. In all cases, follow manufacturers' nailing schedules.

Squash Blocks for I-Joists

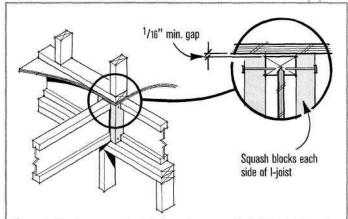
Squash blocks are required under concentrated loads such as posts and, in some cases, where the joists must transfer the load from a bearing wall above to another bearing wall below.

Squash blocks should be slightly larger than the depth of the joists to ensure that they pick up the full load. Fasten blocks to the top and bottom joist flanges with 8d nails (**Figure 42**).

Filler Blocks for I-Joists

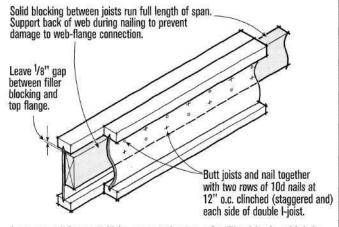
Where two or more I-joists serve as a girder, the web area should be filled in with solid blocking of plywood, OSB, or dimensional lumber. The filler will ensure that both members carry the load.

Figure 42. Squash Blocks



Squash blocks are required to transfer concentrated loads through the floor system at outside walls. They may be used under interior loadbearing walls instead of full-depth blocking between the I-joists.

Figure 43. Filler Blocks



Leave a minimum 1/8-in. gap at the top of a filler block, which is required where two I-joists serve as a beam.

Filler pieces should be a minimum of 4 ft. long, depending on the manufacturers' specs, and should be installed with a gap at the top (**Figure 43**). Nails should be clinched to prevent pullout.

Figure 44. Backer Blocks

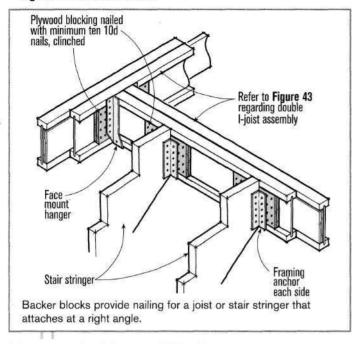
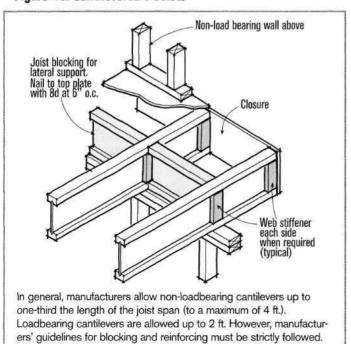


Figure 45. Cantilevered I-Joists



Floor Openings

Where a joist or stair stringer attaches to the side of an I-joist, nail backer blocks to the web to provide a nailing surface. These full-width blocks should extend 6 to 12 in. past either side of the intersecting joist or stringer and may be needed on both sides of the web (**Figure 44**). Refer to the manufacturer's literature for details.

Cantilevered I-Joists

There are several ways to frame cantilevers with I-joists. Most manufacturers permit non-loadbearing cantilevers up to one-third the length of the joist span (to a maximum of 4 ft.). Loadbearing cantilevers may be up to 2 ft. long. Since a cantilever can easily over-stress an I-joist that's not reinforced, it's important to strictly follow the manufacturer's guidelines for allowable spans and required blocking. Figure 45 shows some sample details.

Floors: TRUSSES

Structurally, an open-web floor truss resembles an I-beam in that it puts most of its material along its top and bottom edges where stresses are greatest. To strengthen a truss, the fabricator may double its top and bottom chords, make side-by-side girder trusses, use larger truss plates or stronger wood, or use some combination of these techniques.

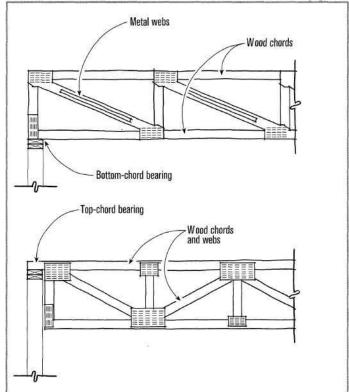
Truss Types

Floor trusses can be designed to sit on either their bottom chord or their top chord (**Figure 46**).

Handling Trusses

When receiving a truckload of trusses, reject those with excessive splits in chords or braces, those with knots close to metal plates, or those with loose or deformed plates. Also reject any that show evidence of having been damaged and repaired. Beware of warped or wet lumber, which can set up dangerous stresses as it shrinks and dries.

Figure 46. Truss Types



Floor trusses typically have either wood or metal webs. **Bottom-chord-bearing** trusses (top) sit atop a wall plate or sill like a standard floor joist. **Top-chord-bearing** trusses (bottom) hang from the top plate.

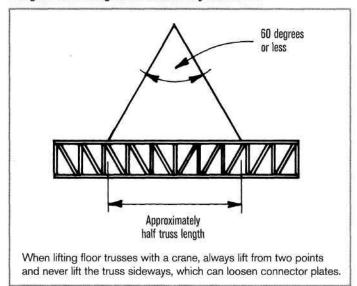
Caution: Loose Plates

Connector plates should be centered over the joint and firmly embedded in the wood. Never refasten a loose plate: The bond cannot be restored once it's been broken.

Lifting With a Crane

If you use a crane, always lift from two points (**Figure 47**) and never lift the truss sideways; the excess flexing can loosen the connector plates, causing eventual failure.

Figure 47. Lifting Floor Trusses by Crane



Installing Floor Trusses

Floor trusses are usually spaced 24 in. o.c., and are typically lifted by hand, rolled into place, fastened, and braced.

Right Side Up

It is crucial to install each truss right side up, according to the label attached to the truss. Each web member is designed to be in compression or tension, but not both.

Bearing at Center Girder

A bottom-chord-bearing truss that crosses a girder or bearing wall may be designed to function as two simple beams. In this case, a tag attached to the truss will indicate that the top chord should be cut after installation (**Figure 48**). Without this cut, a load

Figure 48. Special Field Cuts

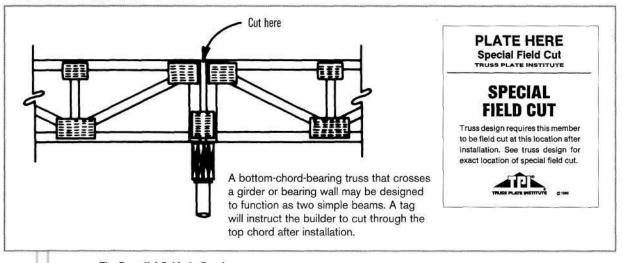
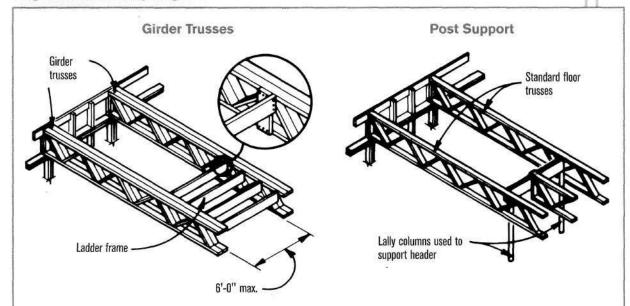


Figure 49. Stairwell Openings



Double-width girder trusses are designed to support several standard floor trusses. These are often used around stairwell openings (left). Another option is to support staircase headers on posts or lally columns (right).

applied to one end of the truss will lift the other, creating a seesaw action.

Stairwell Openings

Girder trusses are designed to support several standard floor trusses. These are often used around stairwell openings (Figure 49).

Bracing Floor Trusses

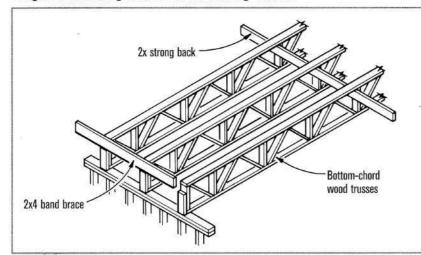
Bracing prevents trusses from bending, twisting, or otherwise deforming. On bottom-chord-bearing trusses, the ends are tied together with 2x4 ledgers

that also serve as a nailing base for the perimeter of the plywood deck (**Figure 50**). Underneath, 2x6 strongbacks laid on edge should run continuously through the webs of all the trusses at 10-ft. intervals (one run for a 20-ft. truss, two runs for longer trusses). The 2x6 serves the same purpose as bridging in a standard floor, distributing concentrated loads over a wider area.

Fire-Stopping for Floor Trusses

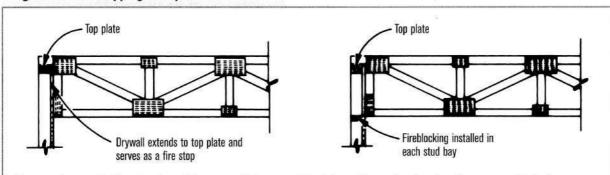
Top-chord-bearing trusses short-circuit the fire-stopping ordinarily provided by the top plate. Common solutions are to extend the drywall past the trusses to the top plate, or to insert a separate 2x4 fire stop inside each stud bay just below the bottom chord of the truss (**Figure 51**). Check with local codes for requirements in your area.

Figure 50. Bracing Bottom-Chord-Bearing Trusses



The ends of bottom-chordbearing trusses are designed to be tied together with 2x4 ledgers that also serve as a nailing base for the perimeter of the plywood deck. In addition, install horizontal 2x6 strongbacks at 10-ft. intervals to distribute loads and prevent twisting, which can loosen truss plates.

Figure 51. Fire-Stopping for Open-Web Trusses



Many codes require fire-stopping with open-web trusses at the intersections of wall and ceiling spaces. Techniques include extending the drywall past the truss to the top plate (left), or installing a 2x4 fire-stop inside each stud bay just below the truss's bottom chord (right).

Walls

Stud Spacing

Maximum stud spacing for Standard or better-grade studs is shown in **Figure 52**. Lower-grade 2x4 studs cannot exceed 16 in. o.c.

Top Plates

Most model codes require loadbearing walls to have double top plates lapped so that the splices are at least 4 ft. apart. Two 16d nails are required on each side of the splice and additional nails are required every 24 in. in the overlap area (Figure 53). See nailing schedules (Figure 16, pages 16-17) for air-nail requirements.

Double vs. Single Top Plates

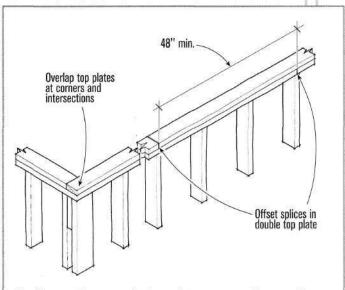
Single top plates are considerably weaker than a traditional double top plate. However, many codes permit single top plates as long as they are joined at splices, corners, and intersecting walls with .036-in.-thick galvanized steel plates, measuring 3x6 in. Plates should be fastened with six 8d nails on each side (six nails for ICBO).

Figure 52. Maximum Stud Spacing (in.)

Stud Size	Supporting Roof and Ceiling Only	Supporting One Floor Roof and Ceiling	Supporting Two Floors Roof and Ceiling	
2x4	24*	16	2 1 35	
2x6	24	24	16	

^{*} Shall be reduced to 16 inches if Utility grade studs are used. Adapted from IRC Table R-602.3(5)

Figure 53. Splicing Top Plates in Bearing Walls



Double top plates must be lapped at corners and intersections, and splices must be staggered at least 48 in. with at least four 16d nails spread across the lap.

Figure 54. Double vs. Single Top Plate

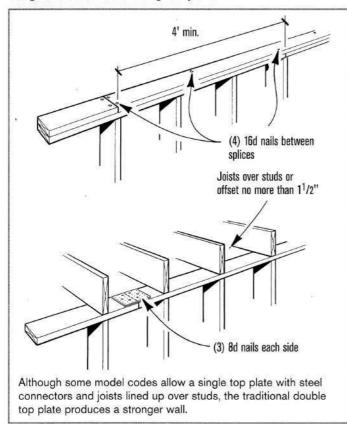
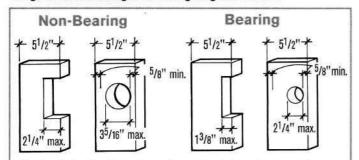


Figure 55. Notching and Boring Regular Studs



Notches in loadbearing studs under 10-ft.-tall should not exceed 25% of the stud depth and should not occur in the middle third of the stud. Bored holes should not exceed 40% of the stud depth and should be at least 5 /8 in. from the edge. See **Figure 9**, page 11 for notching and drilling studs over 10 ft. tall.

When using single top plates, rafters or joists must not be offset from studs by more than $1^{1/2}$ in. (**Figure 54**).

Maximum Stud Lengths

Studs used in exterior loadbearing walls, whether 2x4 or 2x6, should not be more than 10 ft. high without being engineered.

Engineered solutions include reducing stud spacing, using wider studs, doubling the studs, and using studs made from engineered lumber.

Notching and Boring Studs and Plates

Studs

When notching or drilling through studs under 10 ft. tall, follow the guidelines shown in **Figure 55**. Never make notches and holes across from one another in the same section of a stud. For studs over 10 ft. in height, follow guidelines shown in **Figure 9**, page 11.

Plates

If more than 50% of the width of a top plate is notched or drilled away, then the edge of the plate must be reinforced with a 24-gauge steel plate that

spans the distance between the adjoining studs (Figure 31, page 26).

Corner Studs

On three-stud corners, builders often replace the middle stud with wood spacers. While that is acceptable in most cases, the three-stud corner is more than just a nailer for sheathing or dry-wall — it must also transfer shear loads between adjoining walls (**Figure 56**). For this reason, don't omit the third stud where shear resistance is critical.

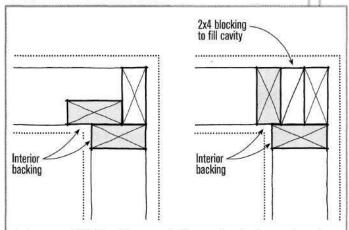
Wall Bracing

In most residential construction, plywood or OSB sheathing panels are used for lateral bracing and are nailed 6 in. o.c. at the edges and 12 in. o.c. in the field. This provides excellent racking resistance. Bracing values for plywood can be improved by using larger nails or by spacing nails more closely together.

Bracing with Foam Sheathing

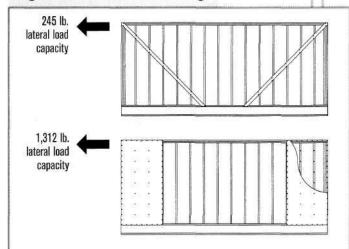
When using a non-structural sheathing such as foam board, install bracing at the building corners to provide resistance to racking. This bracing may consist of diagonal 1x4s or vertical sheets of plywood or OSB (**Figure 57**).

Figure 56. Corner Framing



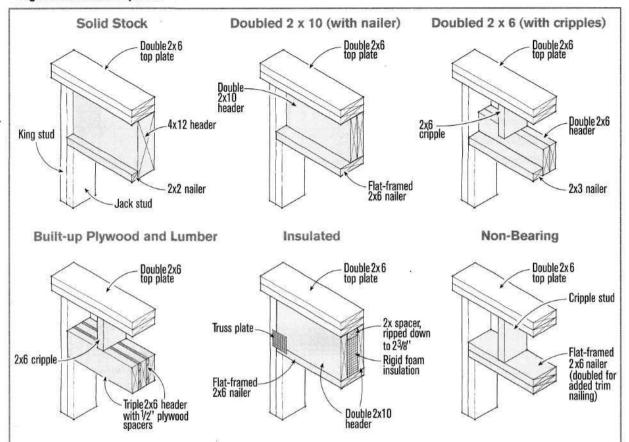
A three-stud "California" corner (left) uses less lumber and can be insulated better than a traditionally framed corner. Never replace the third stud of a three-stud corner with blocks; not only is it a nailer for drywall, but it also provides critical shear strength.

Figure 57. Code-Minimum Bracing



Foam sheathing does not provide adequate racking resistance. However, a pair of ⁷/16-in. plywood braces at each end of the wall will provide more than five times the strength of let-in 1x4s. The plywood should be nailed with 6d common nails 6 in. o.c. on the edges and 12 in. in the field.

Figure 58. Header Options



Using cripples above the header allows for smaller dimension lumber (depending on span requirements), but this option is more labor intensive. To avoid cripples, use 4x12s or 2x12s, or build up to the same depth using 2x10s with an added flat-framed member.

Diagonal bracing. Diagonal bracing is typically notched into the top and bottom plates and all intervening studs, and nailed with two 8d nails at each stud. Use ³/4-in. plywood instead of 1x4s for braces

Metal Bracing

Depending on code, T-shaped metal bracing may sometimes be used in place of wood bracing — typically only as temporary bracing during construction.

Wind Bracing

In earthquake-prone or high-wind areas, pay special attention to the nailing of wall and roof sheathing, as well as to all the vertical framing connections that structurally join the building from foundation to roof. Consult local codes for nailing requirements (see also "Shear Walls," page 74).

Headers

Window and door headers can be framed in a variety of ways, depending on the lumber available and the insulation requirements, as shown in Figure 58.

Header Height

Set headers at the height of door rough openings. For a standard prehung door, the header height needs to be at least 6 ft. 10 in. (**Figure 59**).

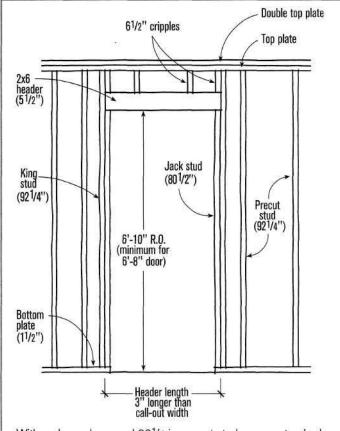
Set window headers at the same height as doors so all openings align.

Rim-joist headers. In a two-story house, rough opening heights can be raised by doubling up on the rim joist, or creating a girder to meet structural requirements for the span (see span tables, pages 98-103).

Sizing Headers

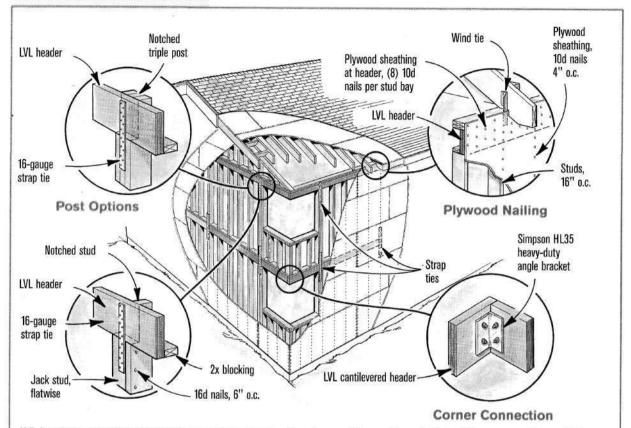
Rough openings in loadbearing walls require headers that are supported at either end by jack studs (trimmers). Header sizes for various house configurations and the number of jack studs required at each end are shown in Figures 60 through 65, pages 98-103.

Figure 59. Header Height



With prehung doors and $92^{1/4}$ -in. precut studs, use a standard $80^{1/2}$ -in. jack stud. (If using $92^{5/8}$ -in. precuts, lengthen the jack stud to $81^{1/8}$ in.)

Figure 66. Cantilevered Headers



LVL headers, securely anchored to the wall framing by strap ties and thoroughly nailed sheathing, are cantilevered above the window opening. For a two-story structure, the lower header may be built-in as the rim joist.

Corner Window Headers

A corner window requires a cantilevered header. **Figure 66** shows the basic building details for such cantilevered headers. To meet actual load conditions, an engineer should specify header dimensions and connection criteria.

Even with proper header sizing, some deflection may occur. Do not nail the

window directly to the header. Manufacturers of corner windows provide metal installation clips to isolate the windows from the rough opening. These clips should be installed using foam backer rod between the header jam and the rough opening. Secure trim to the jamb with a minimal number of light-gauge nails.

Fire-Stopping Details for Walls

In general, residential building codes call for fire stops at the following locations (**Figure 67**):

- In stud walls and partitions at every floor and ceiling level, including furred spaces;
- At every 10 ft. of vertical distance in tall walls or partitions;
- At all interconnections between vertical and horizontal concealed spaces, such as at soffits, cove ceilings, and drop ceilings;
- In the stud spaces along the side of stair stringers;
- At openings around pipes, ducts, chimneys, and fireplaces at floor and ceiling levels.

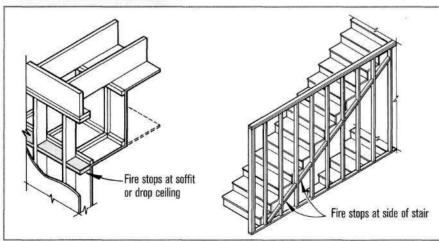
Fire-Stop Materials

Code-approved fire-stop materials include nominal 2-in.-thick lumber, double layers of ³/₄-in. plywood or particleboard (with joints backed by the same material), ¹/₂-in.-thick drywall, and ¹/₂-in. cement board. Unfaced fiberglass batts can be used as fire-stopping under IRC R602.8.1.1 as long the batts fill the stud cavity for at least 16 in. of vertical space.

Irregular Openings

All fire stops should be cut to fit tightly. Voids of more than ¹/8 in. will undermine the material's fire-stopping ability. For irregularly shaped openings, use an "intumescent" fire-stopping compound. Because these products expand when heated, they will fill the void left by plastic piping or cable insulation that has melted away.

Figure 67. Fire-Stop Details



Fire stops are required in walls between floors and wherever concealed vertical and horizontal spaces intersect. Stairwell walls and any walls or partitions over 10 ft. tall also need fire stops.

Roofs: DIMENSIONAL LUMBER

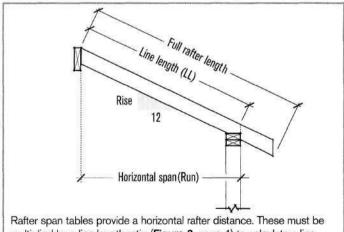
Rafter Loads

Loads on residential rafters typically include snow and wind (the most common live loads), roofing materials, and interior finish materials (dead loads).

Live loading conditions for roofs vary widely with snow and wind loads. Be sure to check local codes for structural design requirements in your area.

For precise dead load calculations, refer to the material weights shown in Figure 22, page 23.

Figure 68. Rafter Span



Rafter span tables provide a horizontal rafter distance. These must be multiplied by a line length ratio (**Figure 3**, page 4) to calculate a line length (sloping distance). Length for plumb cuts and overhang must be added to find full rafter length. Note: The rafter spans in the span tables (pages 104-117) have been shortened for the thickness of the ridge.

Common Rafter Spans

Rafter span is the horizontal distance from bearing at the ridge to bearing at the top plate (Figure 68).

To convert rafter span (horizontal distance) to rafter length (sloped distance), use the conversion factors in Figure 3, page 4.

Maximum rafter spans for common lumber species are given in **Figures 69** to **82**, pages 104-117.

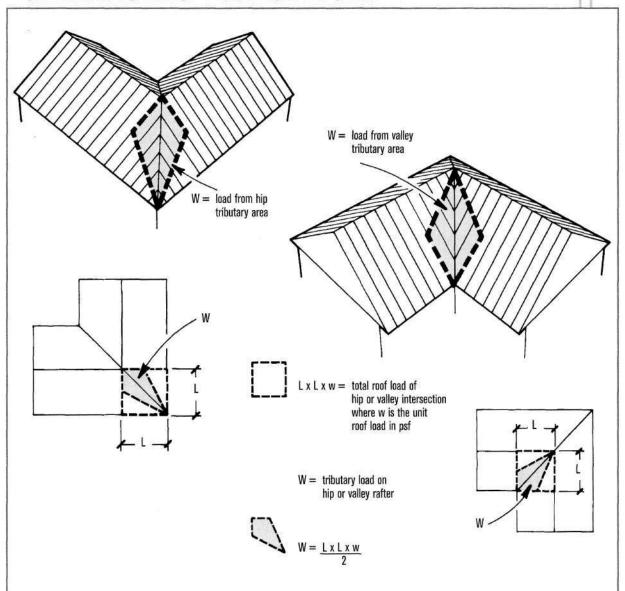
Hip and Valley Rafters

While hip and valley rafters carry significant loads, they are often undersized. To allow for full bearing, hip and valley rafters should be at least one size larger than commons and jacks.

Sizing Hip and Valley Rafters

The loads on hip and valley rafters are *tributary loads* transferred from a wide area of the roof (**Figure 83**). The hip and valley rafter sizing table (**Figure 84**, page 50) accounts for such tributary loads.

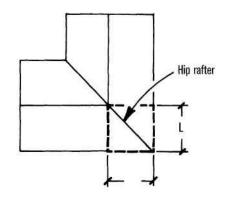
Figure 83. Calculating Tributary Load (W) on Hip and Valley Rafters

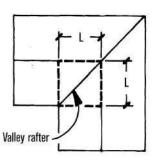


A hip or valley rafter picks up half the load of all the jack rafters feeding into it – its tributary load. In plan view, this tributary load is kite-shaped. Note that the hip's tributary area is wider at the top and the valley's tributary area is wider at the bottom.

Figure 84. Hip and Valley Rafter Sizing Table

L in feet	15 psf live load	30 psf live load	45 psf live load	60 psf live load
4	2x6	2x6	2x6	2x8*
5	2x6	2x6	2x6	2x8
6	2x6	2x8	2x8	2x10
7	2x8	2x10	2x10	2x12
8	2x10	2x12	2x12	(2) 2x12
9	2x10	(2) 2x12	(2) 2x12	(2) 2x12
10	2x12	(2) 2x12	(2) 2x12	LVL 11 ⁷ /8
11	(2) 2x12	(2) 2x12	LVL 11 ⁷ /8	LVL 11 ⁷ /8
12	(2) 2x12	LVL 11 ⁷ /8	LVL 11 ⁷ /8	LVL 14
13	(2) 2x12	LVL 11 ⁷ /8	LVL 14	(2) LVL 14
14	LVL 11 ⁷ /8	LVL 14	(2) LVL 14	(2) LVL 14
15	LVL 11 ⁷ /8	LVL 14	(2) LVL 14	(2) LVL 14
16	LVL 11 ⁷ /8	(2) LVL 14	(2) LVL 14	(2) LVL 16*
17	LVL 14	(2) LVL 14	(2) LVL 16	(2) LVL 16
18	LVL 14	(2) LVL 14	(2) LVL 16	*
19	(2) LVL 14	(2) LVL 16*	*	_
20	(2) LVL 14	(2) LVL 16	(-)	_





*Deflection limited

Note: The calculations behind this table are based on the following:

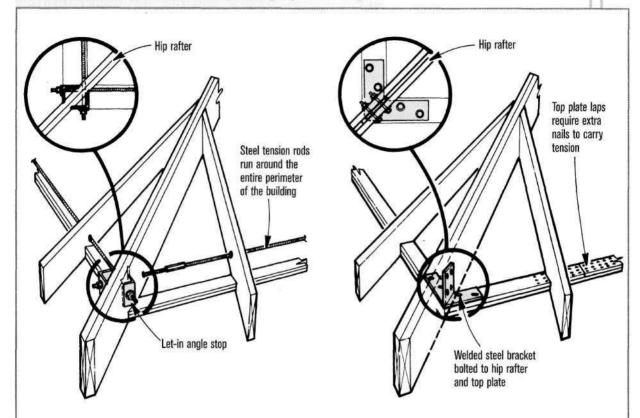
10 psf dead load L/240 deflection F_b wood = 1,000 psi E wood = 1,000,000 psi

No slope adjustments $F_b LVL = 2,800 psi$

E LVL = 2,000,000 psi

The table above summarizes a series of sizing calculations for various roof design loads. L represents the length of a hip or valley rafter for equally pitched roof intersections only.

Figure 85. Apex Support for Cathedral Ceiling Hips and Valleys



In a large hip roof with full cathedral ceilings, there are no support posts or collar ties to resist the spread of the rafters. In such cases, install steel rod tension ties (left) around the perimeter of the building to prevent the bottom ends of the hip rafters from spreading. Alternatively, use welded steel brackets to secure the hip rafters at the corners, allowing double 2x6 top plates to act as tension members (right).

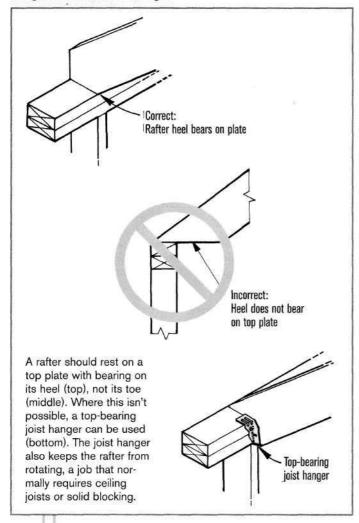
Apex Support

In addition to choosing the right size hip or valley rafter, the point load at the high (ridge) end of a hip or valley must be well supported. Typically, common rafters tied together by ceiling joists or collar ties support this load. Large cathedral ceilings should be engineered to provide adequate support. This may include tension rods along the wall plates or reinforced plate connections for hip and valley rafters (**Figure 85**).

Rafter Bearing

Rafters should have bearing of at least $1^{1}/2$ in. on the top plate or beam. Bearing should be on the heel of the rafter, not the toe. Bearing on the toe places most of the load on only a portion of the rafter and can lead to its splitting (**Figure 86**).

Figure 86. Rafter Bearing



A non-structural ridge board should be at least one size deeper than the common rafters to provide full bearing for the rafter's plumb cut.

Structural Bracing

Rafters must be restrained from spreading. This can be accomplished with adequate connections to ceiling joists, with collar ties, or with a structural ridge beam.

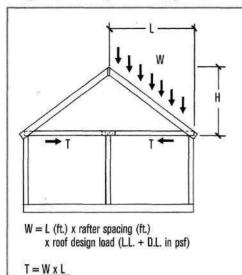
Rafter-Joist Connections

The connection between roof and wall at the eaves needs to resist uplift forces caused by wind (and earthquake activity in seismic zones), as well as horizontal thrust caused by roof loads. Low roof slopes, long rafter spans, and heavy snow loads increase horizontal thrust significantly.

Unless the roof has a structural ridge, the ceiling joists must be continuous across the building and must be fastened to the rafter tails with the number of nails shown in **Figure 87**. If the number of nails is excessive for the amount of nailing area, use bolts or framing clips instead.

A weak link in this system is where ceiling joists join at the center of a building. This connection requires the same nailing schedule as a collar tie-to-rafter

Figure 87. Nailing and Bolting Schedule for Eaves Tie Connections



2H

Roof Pitch	Building Width (2L) 20' 24' 30' 36'					
Pitch				36'		
3/12	T = 1,064 lb.	T = 1,276 lb.	T = 1,596 lb.	T = 1,915 lb.		
	11 nails or	13 nails or	16 nails or	20 nails or		
	3 bolts	4 bolts	4 bolts	5 bolts		
4/12	T = 798 lb.	T = 958 lb.	T = 1,197 lb.	T = 1,437 lb		
	8 nails or	10 nails or	12 nails or	15 nails or		
	2 bolts	3 bolts	3 bolts	4 bolts		
6/12	T = 532 lb.	T = 638 lb.	T = 798 lb.	T = 957 lb.		
	6 nails or	7 nails or	8 nails or	10 nails or		
	2 bolts	2 bolts	2 bolts	3 bolts		
9/12	T = 355 lb.	T = 425 lb.	T = 532 lb.	T = 638 lb.		
	4 nails or	5 nails or	6 nails or	7 nails or		
	1 bolt	2 bolts	2 bolts	2 bolts		
12/12	T = 266 lb.	T = 319 lb.	T = 399 lb.	T = 479 lb.		
	3 nails or	4 nails or	4 nails or	5 nails or		
	1 bolt	1 bolt	1 bolt	2 bolts		

Note: This table is based on 30-pound psf live load plus 10-pound psf dead load. Nails are assumed to be 16d, at 100-pound capacity each; bolts are $^{1}/_{2}$ inch, at 400-pound capacity each. Rafters are 16 inches on-center.

Figure 88. Connecting Flush-Framed Ceiling Joists

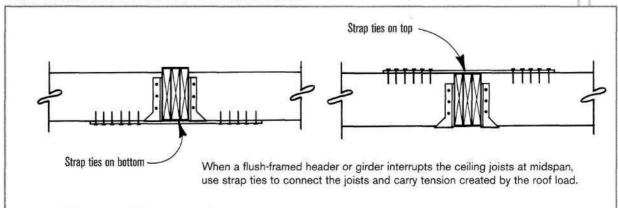
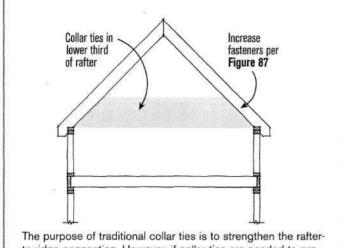
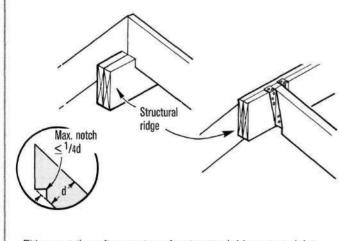


Figure 89. Placing Collar Ties



The purpose of traditional collar ties is to strengthen the rafterto-ridge connection. However, if collar ties are needed to prevent the rafter ends from spreading, then they should remain in the lower third of the span (rule of thumb) or be engineered.

Figure 91. Structural Ridge Connections



Either rest the rafters on top of a structural ridge or use joist hangers attached to the ridge beam. The notch in the rafter should be no deeper than one-fourth its width. connection (**Figure 16**, pages 16-17). When the ceiling joists are in the same plane, as with a flush-framed beam, steel strap ties can be used (**Figure 88**).

Collar Ties

Collar ties often are placed near the ridge, but this placement only serves to strengthen the rafter-to-ridge connection and to stiffen the rafters. To effectively keep rafters from spreading, collar ties must be in the lower third of the rafter (**Figure 89**). They are not necessary if the rafters are adequately nailed to ceiling joists.

Collar-tie connections should be treated like rafter-to-joist connections (**Figure 87**, previous page).

Structural Ridge Beams

In a cathedral ceiling, the outward thrust of rafters is not restrained by ceiling joists or rafter ties and the rafter tops must bear on a structural ridge beam. Sizing for structural ridge beams is shown in **Figure 90**.

Rafters may sit on top of a structural ridge or may be supported by joist hangers or anchors (Figure 91).

Purlins and Roof Struts

Purlins and struts can be used to reduce rafter spans or to stiffen rafters (Figure 92). To properly support the roof, the purlins should be at least the same dimension as the rafters while the struts should transfer the load to a bearing wall at an angle not less than 45 degrees. The IRC 2000 sets the maximum spacing of 2x4 struts at 4 ft. o.c.

Figure 92. Purlin Design

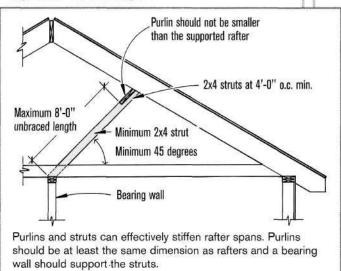


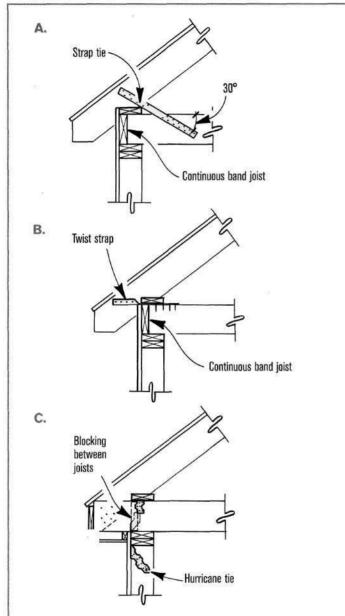
Figure 90. Structural Ridge Beam Spans for 20 psf Roof Live Load

	Roof	Dead Load =	10 psf	Roof I	Dead Load =	20 psf	
	Building Width (ft.)			Building Width (ft.)			
	20	28	36	20	28	36	
Size	Maximum Ridge Beam Spans for Common Lumber Species (ftir						
1-2x6	4-10	4-1	3-7	4-2	3-6	3-1	
1-2x8	6-1	5-2	4-7	5-3	4-6	3-11	
1-2x10	7-5	6-4	5-7	6-5	5-5	4-10	
1-2x12	8-8	7-4	6-5	7-6	6-4	5-7	
2-2x6	7-2	6-0	5-4	6-2	5-3	4-7	
2-2x8	9-1	7-8	6-9	7-10	6-7	5-10	
2-2x10	11-1	9-4	8-3	9-7	8-1	7-2	
2-2x12	12-10	10-10	9-7	11-1	9-5	8-3	
3-2x8	11-1	9-7	8-5	9-10	8-4	7-4	
3-2x10	13-10	11-8	10-4	12-0	10-2	8-11	
3-2x12	16-1	13-7	12-0	13-11	11-9	10-4	
4-2x8	12-3	10-11	9-9	11-1	9-7	8-5	
4-2x10	15-7	13-6	11-11	13-10	11-8	10-4	

^{*} Tabulated values assume #2 Grade Douglas Fir-Larch, Hem-Fir, Southern Pine, or Spruce-Pine-Fir lumber.

Cathedral ceilings require structural ridge beams. This table shows two dead loading conditions (10 and 20 psf) under live load conditions of 20 psf. In areas with heavier snow and wind live loads, stronger ridge beams will be required. For longer spans and heavier loading conditions, consider using LVL or other engineered materials.

Figure 93. Raised-Rafter-Plate Connections



Using rated strap ties (A) is an effective way to resist roof thrust and uplift on raised rafters. When an attic floor is in the way, twist straps (B) will work, but may require additional wind ties in high wind areas. Extending the attic joist beyond the wall (C) allows for hurricane ties to help resist uplift.

Raised Rafter Plates

To create added space for insulation at the eaves, many builders raise the rafters up and fasten them to a plate nailed to the top of the ceiling joists.

While this reduces heat loss and ice dams, it also weakens the important connection between the ceiling joists and the rafter ends, thereby requiring reinforcement (Figure 93).

Blocking for End Restraint

Rafter ends connected to ceiling joists are generally not at risk of rotating. But where rafters sit on a beam or plate by themselves or are raised above the joists, full-height blocking should be installed between the rafters or a rim joist (or subfascia) should be nailed to their ends.

Blocking is often needed to close off open eaves (no soffit), but not for structural reasons.

Overhangs

In general, roof overhangs should not exceed 2 ft. or one-third the horizontal span of the rafter, whichever is less (Figure 94).

Rake Overhangs

There are two common ways to build overhangs at rakes:

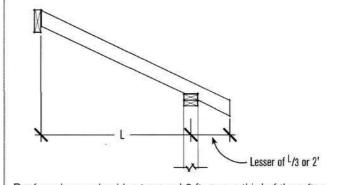
- For overhangs shorter than 1 ft., blocks nailed to the gable-end wall are adequate.
- For larger overhangs, short "outlookers," or purlins, are typically cantilevered (Figure 95). These should not cantilever more than 2 ft. or half the span of the purlin, whichever is less.

Roof Openings

In general, at roof openings more than 4 ft. wide, both headers and trimmers

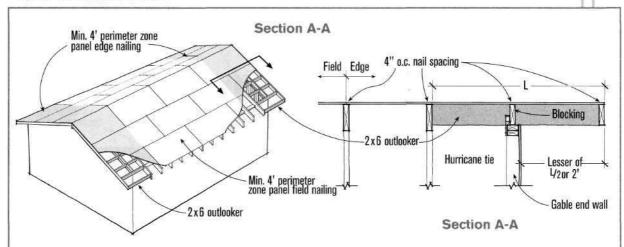
should be doubled. At openings more than 6 ft. wide, joist hangers should support headers unless they bear on a supporting beam or wall.

Figure 94. Roof Overhangs



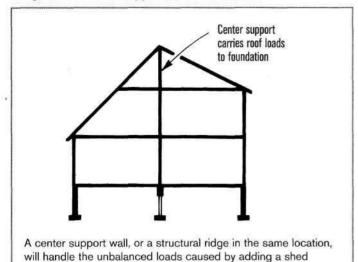
Roof overhangs should not exceed 2 ft. or one-third of the rafter span, whichever is less.

Figure 95. Rake Overhangs



Outlookers at the rake should not exceed 2 ft. or half the span of the outlooker, whichever is less. Blocking-type outlookers should not exceed 1 ft. In high-wind areas, nailing of the sheathing around the roof's perimeter may need to be upgraded.

Figure 96. Center Support for Shed Dormers



Shed Dormers

Adding a shed dormer to a typical gable roof upsets the balance of forces by breaking the stable triangle formed by the rafters and ceiling joists.

Two common ways to support the dormer loads are with a center loadbearing wall (**Figure 96**) or a structural ridge. Either solution must provide a continuous load path to the foundation.

Shed Dormers With Structural Ridges

A structural ridge can replace the ridge or can be installed beneath it (**Figure 97**).

Figure 97. Retrofit Ridge Connections for Shed Dormers

dormer. The loads must follow a continuous path to the footing.

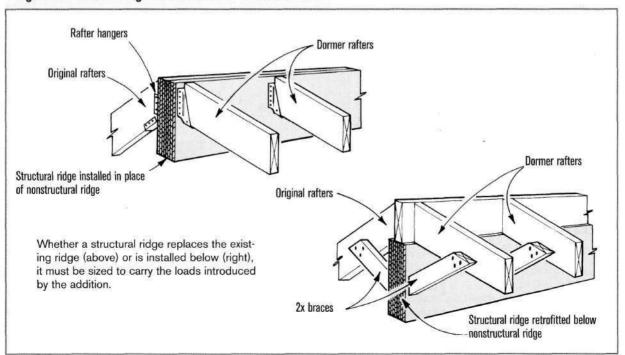
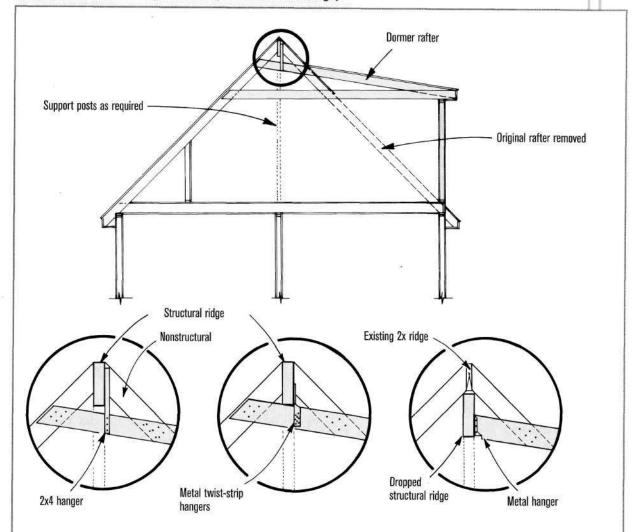


Figure 98. Dropped-Ridge Dormer (with Structural Ridge)

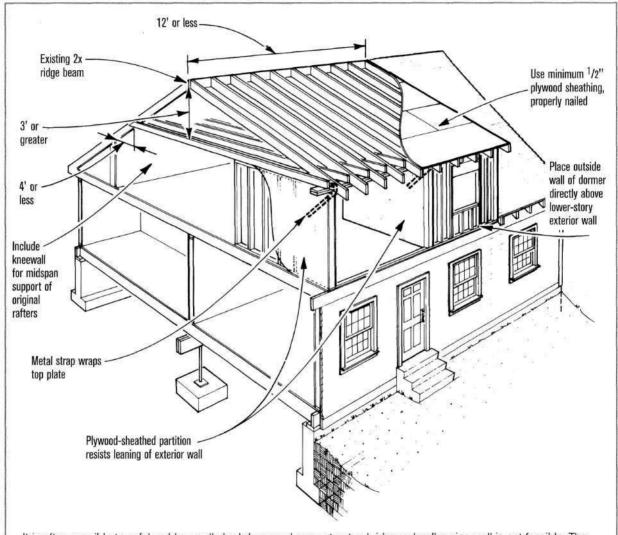


Where the dormer ridge is dropped below the main ridge, the dormer ridge must be tied securely to the structural ridge or center loadbearing wall. Several options are shown.

Where a structural dormer ridge is dropped, it should tie in securely to the structural ridge or center loadbearing wall (Figure 98).

With no structural ridge or center loadbearing walls, small shed dormers are still possible but a combination of structural elements must be added (Figure 99, page 60).

Figure 99. Precautions for Small Shed Dormers



It is often possible to safely add a small shed dormer where a structural ridge or loadbearing wall is not feasible. The precautions shown here offer general guidelines that can work together to support the dormer and to prevent the ridge from sagging and the dormer wall from leaning.

Roofs: WOOD I-BEAMS

I-beams are being used more often in roof framing, particularly on cathedraltype ceilings with long spans.

Structural Ridge Required

All I-beam roofs require a center loadbearing wall or a structural ridge beam, since there is no practical way to make a strong shear connection at the rafter ends to resist horizontal thrust.

Structural Ridge With Hangers

The most common connection at the ridge is a face-mounted hanger with a sloped seat. These hangers can be adjusted in the field to match the I-beam slope, and can be skewed side-to-side up to 45 degrees for hip and valley jack rafters.

Install beveled web-stiffeners on each side of an I-beam where it sits in the hanger. Leave a ½-to ½-in. gap at the top flange and secure the stiffeners by driving three or more 8d nails from each side, staggered and with the points clinched. Larger I-beams may require 2x stiffeners with 16d nails. In

Figure 101. Structural Ridge Connections

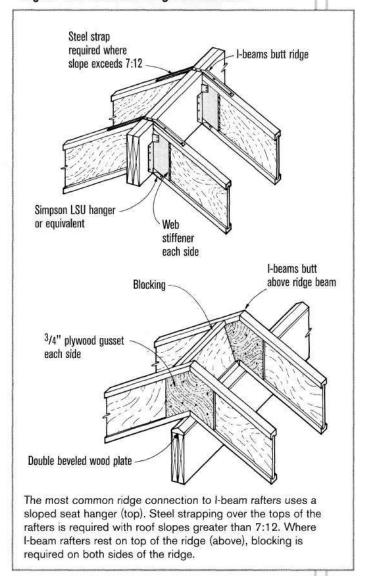
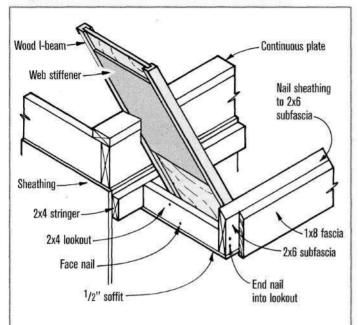


Figure 102. Birdsmouth Cut for I-Beam Rafters



With a birdsmouth cut, it is critical that the entire bottom chord bear directly on the top plate. Provide web stiffeners and lateral bracing – metal cross bracing, dimensional lumber, engineered rim joist material, or I-beam material – on both sides of rafter.

all cases, follow manufacturers' nailing schedules.

Structural Ridge Below Rafters

I-beams can sit on top of a structural ridge on a beveled plate (**Figure 101**, previous page). Never cut a birdsmouth in the I-beam at the ridge — this would require cutting though the bottom flange, thereby damaging the joist.

To prevent rafters from rolling, install blocking between the I-beams on

either side of the ridge. The blocking can be I-beam material, dimensional lumber, or metal cross-bracing. If you need to leave room for a ventilation channel, use dimensional lumber or engineered rim joist material notched to allow airflow, or use metal cross-bracing.

Eaves Connections

A number of details are possible at the exterior wall plate, depending on the roof profile desired.

Birdsmouth for I-Beam Rafters

The most common approach to joining I-beam rafters to walls is to cut a birdsmouth at the plate. The seat must never overhang the inside face of the bearing wall, otherwise the I-beam will be compromised. Web stiffeners are required on both sides of the birdsmouth cut (**Figure 102**).

Beveled Wall Plates for I-Beam Rafters

I-joist rafters can sit on a beveled top plate (**Figure 103**). This option can save time since no birdsmouth or web stiffeners are required.

Blocking between rafters is required when using beveled wall plates. For blocking, use either I-beams, dimensional lumber, or metal cross-bracing. Some I-beam manufacturers may require additional connectors on roofs with steep slopes.

Sloped Seat Connectors

A third option to connect I-beam rafters to walls is to use sloped-seat metal connectors. As with the beveled-plate approach, these do not require a birdsmouth or web stiffeners, but do require blocking between rafters.

I-Beam Overhangs

Because cutting through the bottom flange compromises the strength of an I-beam rafter, rafter tails with birdsmouths are limited to a 2-ft. horizontal projection (Figure 104).

Soffits

There are several ways to build traditional soffits. One common approach is to attach 2x4 blocking to the I-beam rafter tails as shown in **Figure 102**. Another option is to sister on rafter tails of dimensional lumber.

Gable-End Overhangs

For an overhang at the gable end, cantilever dimensional lumber outriggers across the rake-wall top plate (**Figure 105**). These are similar to the outriggers used in stick framing (**Figure 95**, page 57).

Figure 103. Beveled Wall Plates for I-Beam Rafters

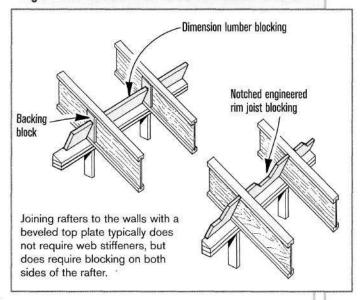
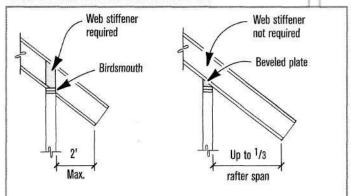
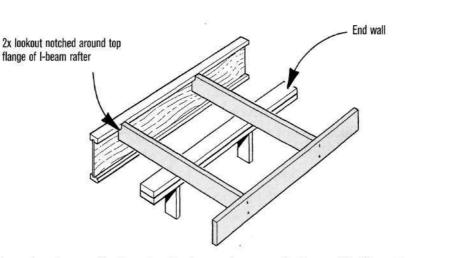


Figure 104. I-Beam Rafter Tails



With a birdsmouth (left), the overhang for an I-beam rafter is limited to 2 ft. of run. With a beveled top plate or sloped hanger, the overhang may be as long as one-third the length of the rafter (right).

Figure 105. Rake Wall Overhangs



Frame rake-wall overhangs with dimensional lumber outriggers notched around the I-beam top flange. If the overhang exceeds the I-beam spacing, check with the manufacturer to see if a double I-beam is required.

Temporary Bracing for I-Beams

I-beam rafters (like floor I-joists) are unstable until fully braced and sheathed. It's crucial to install all blocking and provide lateral restraint before applying any weight to the rafters. As with floor I-joists, stabilize an unbraced end by installing the first 4 ft. of sheathing, then brace the rest of the rafters with 1x4 braces nailed flat to the top of the I-beam rafters every 6 to 8 ft. and lapped at the ends by at least two joists.

Roofs: TRUSSES

The main components of a truss are shown in Figure 106. Roofs framed with trusses are engineered systems. They must be installed and braced properly to work as planned. Any changes from the original plan in bearing or loading or any field modifications to the trusses must be engineered.

Truss Types

Many types of standard trusses are now produced and almost any roof design can be custom fabricated. The most popular types of trusses are shown in Figure 107.

Truss Overhangs

When ordering trusses, specify the span, slope, width of the bearing walls (2x4 or 2x6), and the length and type of overhang (**Figure 108**).

Figure 106. Truss Components

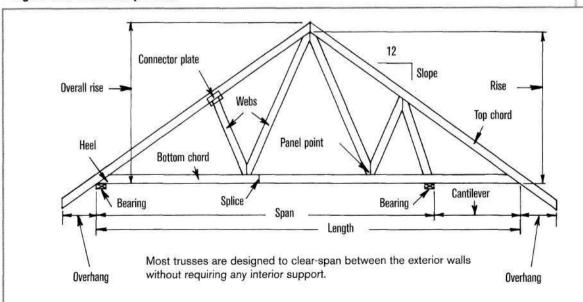


Figure 107. Truss Types

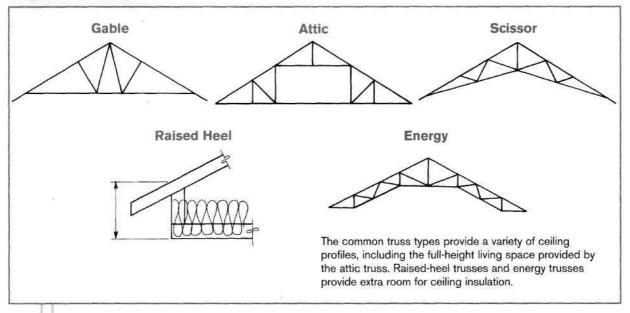
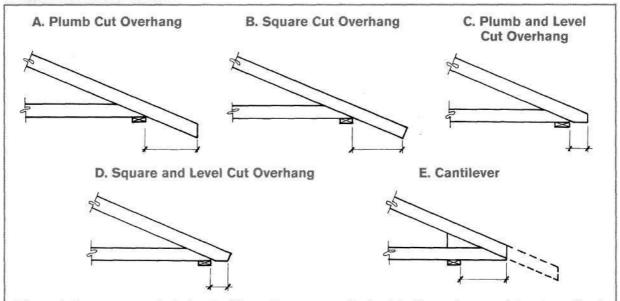
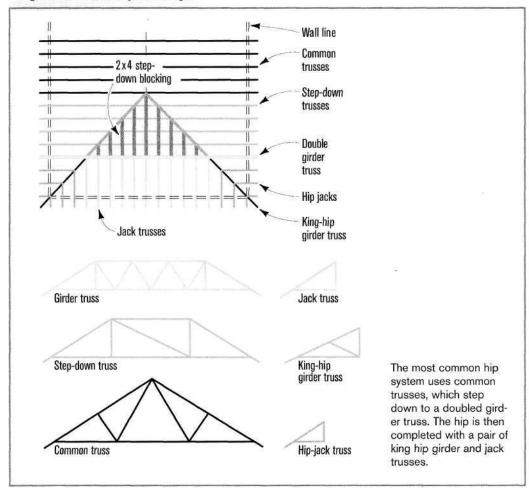


Figure 108. Truss Overhangs



When ordering trusses, specify the length of the overhang, measured horizontally. The overhang usually is not considered part of the truss length; only cantilever overhangs (E) are included in the truss length. In addition, be sure to call out how the top chord is cut at the end (A, B, C, or D).

Figure 109. Truss Hip Anatomy



The truss length is typically the length of the bottom chord; it does not include the overhang, which is most often a projection of the top chord.

Hip and Valley Trusses

Hip roofs and valleys between intersecting roofs may be built around an assembly of jack trusses attached to a girder truss.

Hips. Step-down trusses complete the upper end of the hip series and smaller trusses fill in the lower corners (Figure 109). As with other trusses, it's critical that the dimensions of the building match the drawing and that walls are square and level.

Valleys on a trussed roof are usually framed conventionally. However, when a project includes more than one valley of the same size, a valley set may be more economical (Figure 110).

Figure 110. Valley Sets

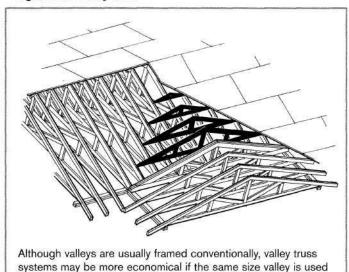
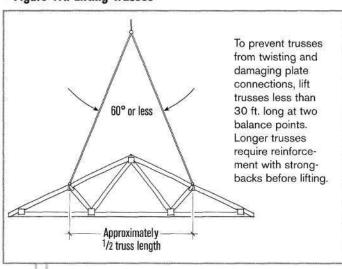


Figure 111. Lifting Trusses

more than once in a project.



The Essential Guide to Framing

Handling and Storing Trusses

Trusses are vulnerable to damage until they are installed, sheathed, and braced. To prevent damage, use the following precautions:

- Inspect trusses when receiving a shipment. Look carefully for loose plates and reject any damaged trusses.
- Banded trusses should be lifted off the truck from two points on the top chords. Individual trusses should be lifted the same way (Figure 111).
- Store trusses horizontally on relatively level, dry ground. To prevent any bending or twisting that could loosen truss plates, support the trusses with blocking placed every 8- to 10-ft.
- If trusses must be stored vertically, make sure they are braced and blocked in a stable manner. Gable trusses should be stored with their peaks up, scissors trusses with their peaks down.

Bracing Roof Trusses

Trusses are inherently unstable until sheathed and require two types of bracing: temporary and permanent.

Use temporary bracing to safely erect the trusses; permanent bracing is required to stabilize the trusses throughout the life of the structure. The truss fabricator or "designer of record" should provide a permanent bracing plan.

Usually some of the elements of the temporary bracing stay in place as part of the permanent bracing. In general, all bracing should be placed near panel points (where truss members meet).

Temporary Bracing: The First Truss

It is important to accurately plumb the first truss and to brace it substantially, since additional trusses rely on the first one for stability.

All bracing must be of 2x material.

Start with the gable-end truss. Most builders start by sheathing the gable-end

Figure 112. Bracing to the Deck

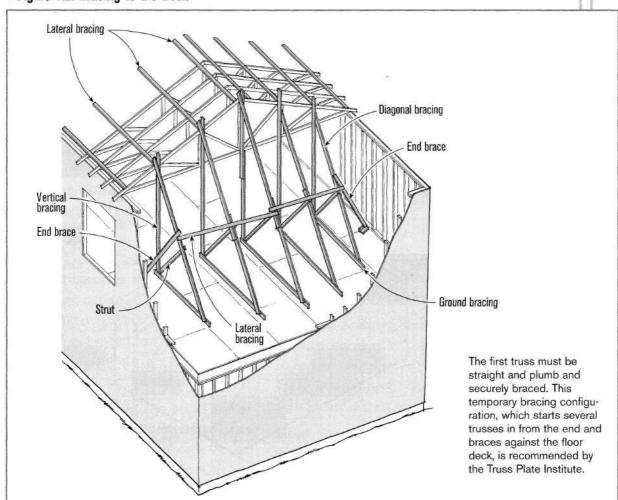
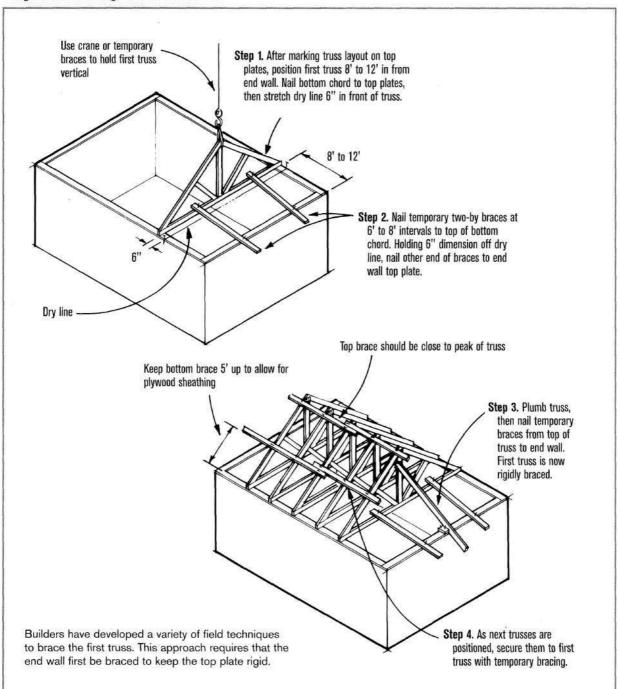


Figure 113. Bracing to the End Wall



truss on the ground and lifting that first. Unfortunately, the gable-end truss is difficult to brace back to the deck without the braces interfering with the second truss. On a one-story building, the gable-end truss can be braced to stakes driven in the ground.

Start several trusses in. Alternatively, start the first truss 8- to 12-ft. in from the gable end and brace it to the deck (Figure 112, page 69). Then work away from the braced end, filling in the open 8- to 12-ft. section last, after permanently bracing the rest of the trusses.

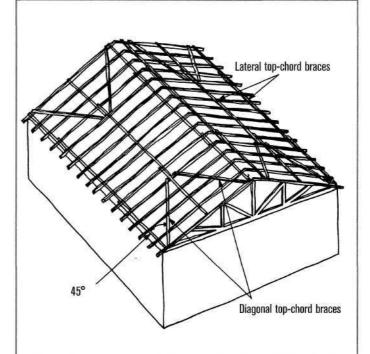
Or brace the trusses to an end wall (Figure 113). It may first be necessary to solidly brace the end wall to the deck to keep the top plate rigid.

Temporary Bracing: Subsequent Trusses

Spacers. As trusses are added to the roof, they can be spaced from the preceding truss with short 1x4 or 2x4 spacers pre-cut to length, with light-gauge metal spacers or with heavy-duty fold-out metal braces. (The heavy metal braces can also serve as temporary lateral bracing for the top chord.)

Top-chord bracing. As soon as the fourth truss is up, start fastening lateral bracing across the top chords — one brace near the peak and one near the midpoint of each top chord. If

Figure 114. Diagonal Top-Chord Bracing



Diagonals are recommended to prevent racking until the sheathing is applied. Some builders place the lowest lateral bracing at least 4 ft. up to allow room for the first layer of plywood.

required, place diagonal bracing at each end of the roof and at 20-ft. intervals in between (**Figure 114**).

All lateral bracing should be minimum construction-grade 2x4s, at least 10 ft. long and nailed with two 16d nails at each intersection. Individual pieces should lap at least one bay.

Roof sheathing. To quickly stabilize the top chords, some builders start installing sheathing after about a dozen trusses have been installed. The sheathing acts as both temporary and permanent bracing for the top chords.

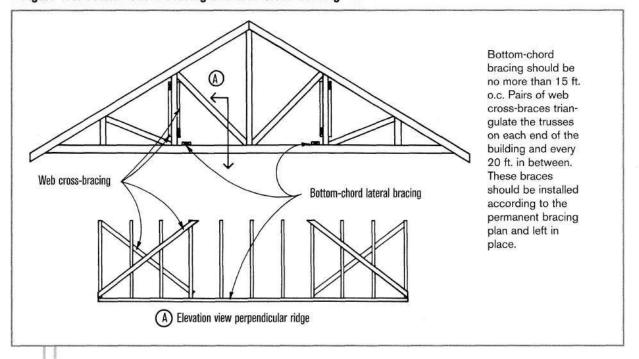
To simplify installation of the sheathing, some builders keep the lower topchord braces 5 ft. up from the eaves line to allow room for the first course of sheathing. Unless the sheathing is installed shortly after erecting the trusses, diagonal top-chord braces may be needed to prevent racking in the roof or truss collapse.

Bottom-chord bracing. After the fourth truss is up, also start installing lateral bracing on the bottom chord (along its top edge if the bottom

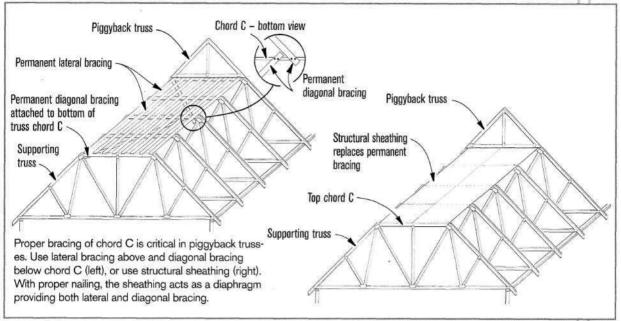
chords are receiving drywall). Install bottom-chord bracing according to the permanent bracing plan and leave in place. On large trusses, diagonal bottom-chord bracing may be required at each end and at 20-ft. intervals in between.

Web cross-bracing. After the fourth truss is up, also start fastening diagonal cross-bracing to the vertical webs. Cross-bracing of the vertical webs goes in an X pattern at each end of the building and every 20 ft. in between (Figure 115). Install web cross-bracing according to the permanent bracing plan and leave in place.

Figure 115. Bottom-Chord Bracing and Web Cross-Bracing







Permanent Truss Bracing

To perform as designed, roof trusses require permanent bracing after assembly, as specified by the "designer of record" on the job. In the absence of an architect or engineer, this responsibility may fall to the general contractor.

Permanent bracing typically consists of many of the same elements as the temporary bracing (see above), most of which are left in place after construction. One exception is any top-chord bracing, which must be removed to allow installation of the roof sheathing. The roof sheathing then serves as permanent top-chord bracing.

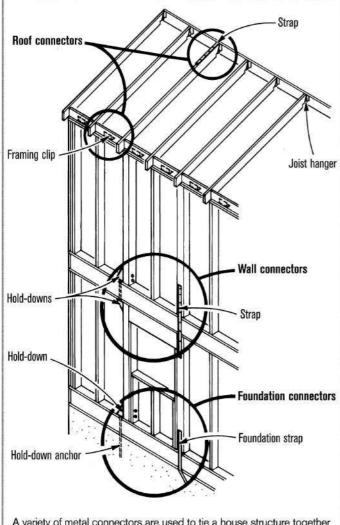
Piggyback Trusses

When trusses exceed 12- to 14-ft. in height, they are typically shipped in two sections to comply with highway transportation limits. These so-called "piggyback trusses" have special bracing requirements. Ignoring these requirements can lead to catastrophic failure under heavy loads such as snow.

In particular, it is critical to stabilize the top chords of the lower truss sections with either plywood or diagonal bracing (**Figure 116**). Other permanent bracing may also be required.

Framing: SEISMIC AND WIND BRACING

Figure 117. Hold-Down Paths



A variety of metal connectors are used to tie a house structure together and create a continuous "hold-down" path from roof to foundation.

High winds exert strong lateral forces on walls and uplift forces on roofs. Earthquakes also exert strong lateral forces, along with vertical shaking and other damaging forces. To help buildings in affected areas resist these forces, codes require that they have sufficient shear strength and have a continuous "hold down" path from roof to foundation (Figure 117). Metal connectors are typically required at the weak points between foundation and first floor, at level changes, and where upper walls join roofs. The details and hardware needed are similar in both seismic and high-wind areas.

Shear Walls

Continuous plywood across wall planes and tighter nailing schedules are crucial elements of structural design for seismic and high-wind areas.

Shear Wall Nailing

Shear walls are designed to resist racking. Both interior and exterior shear walls have rigorous nailing schedules,

Figure 118. Typical Shear Wall Details

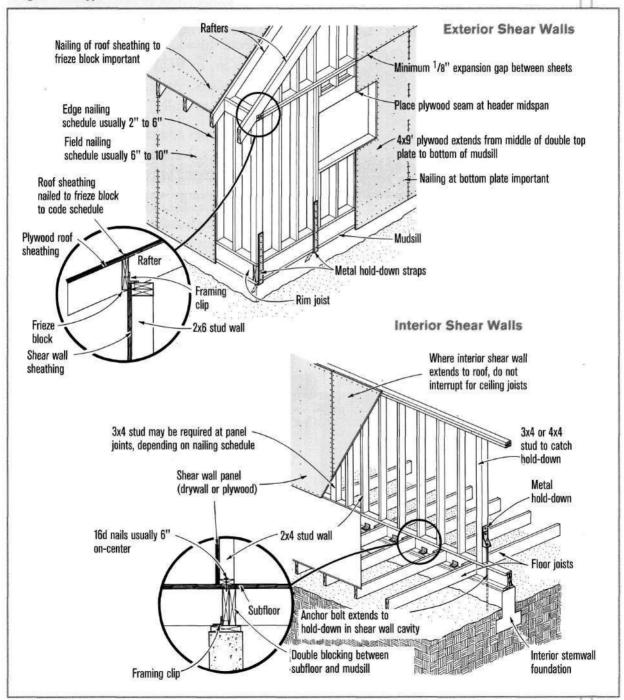


Figure 119. Proper Nailing at Shear Panel Joints

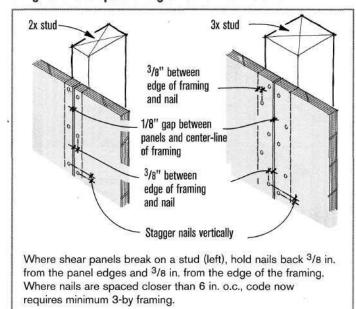
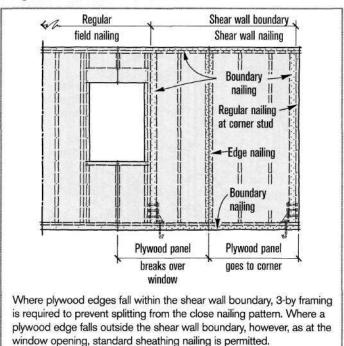


Figure 120. Shear Wall Boundaries



with nails spaced only 2- to 3-in. apart on panel edges (Figure 118, previous page). Nails must be held back ³/8 in. from the edges of sheathing panels and ³/8 in. in from the edges of framing members. Also, they must be staggered vertically (Figure 119).

Nail types and sizes are also specified. While galvanized nails can be used, they have lower shear values and require larger nails or closer spacing.

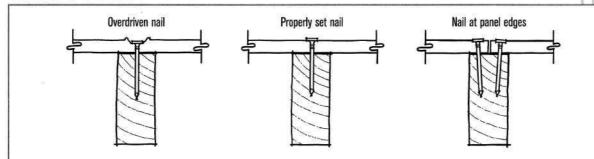
Nail heads must be large enough and must not be over-driven (Figure 121).

Shear Wall Blocking

Because shear forces are transferred at panel edges, all edges of plywood and other sheathing panels must be fastened to solid blocking. Many builders use 4x9 or 4x10 plywood panels installed vertically (**Figure 118**, previous page).

Where sheathing panels meet, each edge must have at least 1/2 in. of bearing on the stud, plate, or other member it is nailed to. Where the design shear exceeds 350 lbs. per foot (typically, where nails are spaced closer than 6 in. o.c.), the Uniform Building Code requires minimum 3x lumber at the joint. Most builders use 4x4s (Figure 120).

Figure 121. Setting Nails



A nail that ruptures the outer plies of the panel (left) has less shear strength. A properly set nail should either sit snuggly on top of the plywood (center) or slightly dimple the outer ply. When panels break on a stud, set the nails at a slight angle to ensure proper embedment in the framing (right).

Anchoring to Foundations

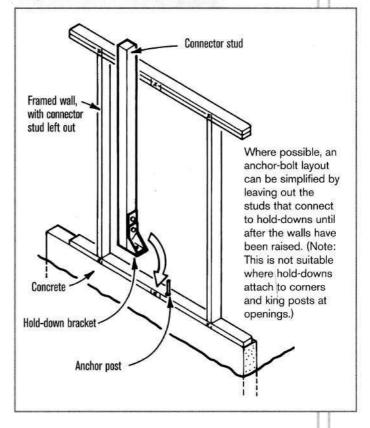
All shear walls must be mechanically fastened to the foundation with metal hold-downs, metal straps, closed-space anchor bolts, or some combination of these.

Hold-Downs

These L-shaped brackets attach to anchor posts (anchor bolts) embedded in the foundation. For studs in a wall without openings, it's often best to install the studs that connect to the hold-downs after the wall is raised (Figure 122).

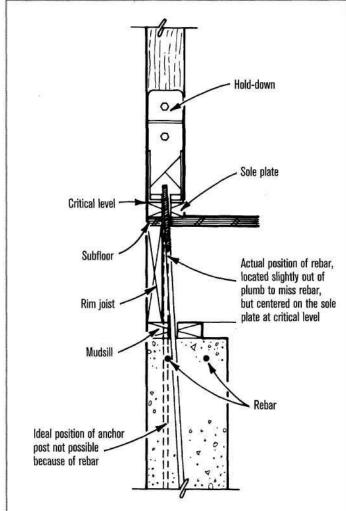
Where anchor posts attach to a corner stud or at one side of a wall opening, they must be located precisely. If possible, wire the anchor posts directly to the rebar. If the rebar is in the way, it

Figure 122. Hold-Down Installation



may be necessary to install the anchor posts slightly out of plumb (Figure 123).

Figure 123. Out-of-Plumb Anchor Bolts



An anchor bolt may be slightly out of plumb if rebar is in the way. This will not affect the strength of the hold-down, but be sure the top end of the bolt is still centered where it comes through the sole plate.

Strap Anchors

These concrete-embedded metal straps nail or bolt to the face of the stud. Because they usually require no drilling, they are easier to install than hold-downs. However, they have significantly lower design loads. Also, the studs they nail to may split under the heavy nailing required. If so, replace the stud with a double stud or 4x member.

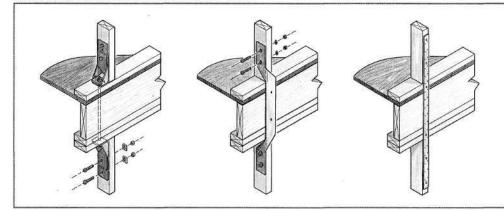
Stacked Wall Connections

There are several ways to reinforce the connection between floors (**Figure 124**). The most common approach for seismic work uses a pair of hold-downs with a large threaded rod between them. Other approaches use straps nailed directly to the studs or through the sheathing. In all cases, the studs must be aligned between floors. With metal straps, some builders use 4x4s because they are less prone to splitting with the large number of nails.

Roof Connections

Winds can exert strong uplift forces. Roofs with low slopes or large overhangs are more susceptible to these forces. Minimum code nailing schedules are rarely adequate to resist these forces.

Figure 124. Floor-to-Floor Connections



To provide a secure load path between stories, engineers specify bolted hold-downs, with the lower one turned upside down (far left), or straps that bolt (center) or nail to the studs (near left).

Adding wind ties, hurricane anchors, or other steel connectors at eaves connections is often required, and is good insurance in high-wind areas.

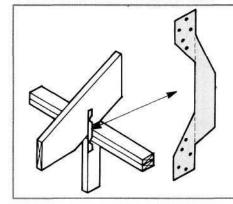
Framing Clips

A common detail in seismic zones is to connect the frieze block to the double top plate with a metal framing clip (**Figure 118**, exterior wall inset, page 75). These must be installed before the roof sheathing.

Hurricane Anchors

In high-wind areas, hurricane clips or rafter ties may be required to connect rafters or trusses to top plates (**Figure 125**). As with all rated connectors, the manufacturer's nailing schedule must be followed.

Figure 125. Eaves Connections



Nailing rafters to plates and plates to studs is not always enough to resist high winds. Some codes call for adequately rated hurricane anchors or rafter hold-downs at 4-ft. intervals in areas of high winds.

Ridge Connections

Steel connectors also may be required to reinforce the rafter connection at the ridge (**Figure 117**, page 74). These may consist of joist hangers installed at the ridge beam or rated steel straps placed across the tops of the opposing rafters. As with other strap connectors, nailing into 2x material may be a problem due to the number of fasteners.

Energy-Tight Details

Figure 126. Insulating the Rim Joist

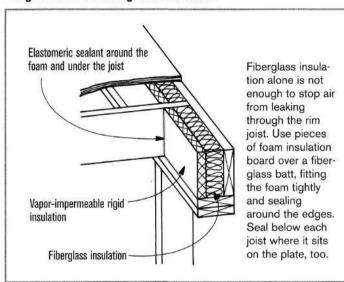
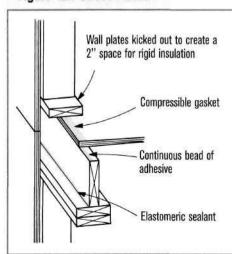


Figure 127. Offset Plates



Keeping the rim joist warm is critical in cold climates where condensation can accumulate on cold framing. This is best done by offsetting the wall plates to provide a channel for insulation board around the perimeter.

Energy codes focus on air-sealing details, vapor barriers, and standard insulation values throughout the house. Good framing practice helps to ensure there is an adequate amount of insulation in all corners of the exterior shell. In addition, slight alterations in practice can make it easier to install a continuous air/vapor barrier on the inside of the house, as required by most energy codes in the U.S.

Sealing the Rim Joist

The rim joist is one of the greatest sources of air leaks in a wood-frame house. However, it is also one of the most difficult places to seal effectively.

The most common way to address this difficult area is to seal and insulate it after framing (Figures 126). Do not just stuff fiberglass into each joist bay. Foam insulation board, sealed tightly on all four sides, must be used to stop the flow of air and vapor.

When done thoroughly, fitting foam into each joist bay is time-consuming, so it's actually easier to address this area at the framing stage by offsetting the wall plates (**Figure 127**). This provides a 1½-2 to 2-in. cavity for strips of foam insulation board. Seal the corner between the rim joist and the bottom plate with urethane caulk and apply continuous beads of construction adhesive when installing floor sheathing and exterior walls.

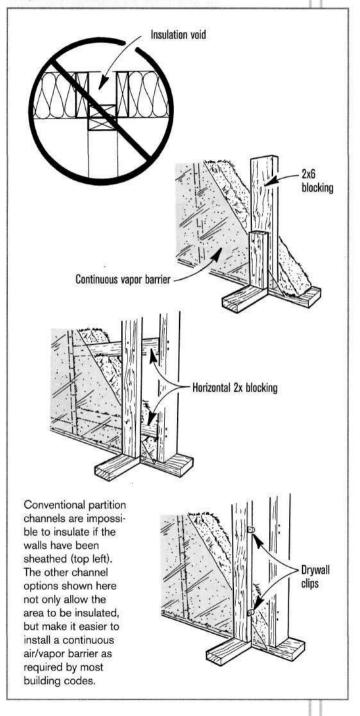
Partition Channels

Interior partition channels in framed walls often create voids, which are inaccessible once the exterior walls are sheathed. Figure 128 shows several ways wall channel can be detailed to provide an easily accessible insulation bay. To provide a continuous air/vapor barrier on the exterior walls, insulate and install a poly vapor barrier before standing the interior walls.

Sealing Knee Walls

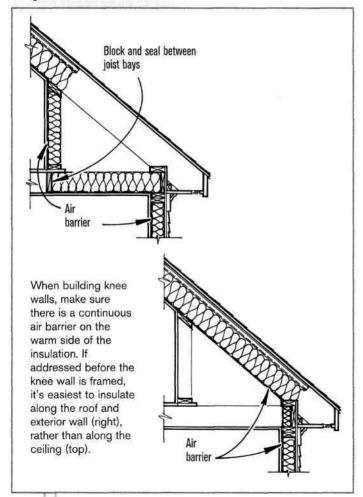
The knee walls in a story-and-a-half Cape often create gaps in the insulation and/or in the air/vapor barrier. There are two common ways to insulate the knee wall area (both shown in Figure 129, page 82):

Figure 128. Interior Wall Channels



Follow the wall and floor. The more difficult way is to insulate the knee wall and the floor of the knee-wall area. Install a poly air/vapor over the insulation of the knee wall, as well as on the ceiling area below, taping it to an air block (foil-faced foam works well) between the joists just below the knee wall.

Figure 129. Knee Walls



Follow the roof. An easier way to handle knee walls is to insulate the roof all the way down to the exterior wall — including a continuous vapor barrier on the inside face of the rafters — and then build the knee walls later. This works especially well if the knee-wall cavity will be used for storage. In this case, however, it's critical that the rim joist be sealed using foam board, as well.

Sealing Cantilevers

Many Colonial-style houses have a section of second floor cantilevered over the first-story wall. Without proper attention, this area can lose a lot of heat.

Keep track of the barrier. During construction, treat cantilevered floors like the floor-knee-wall transition, but install the vapor barrier on the subfloor of the second floor (Figure 130). Where the poly air barrier on the wall meets the floor, tape the plastic to the plywood. Then seal all the seams in the plywood subfloor with tape or caulk—that way, the plywood will function as an effective air barrier on the warm side of the insulation.

Block airflow at the floor. Between the cantilevered floor joists, fill the voids completely with fiberglass or cellulose insulation. Then install rigid foil-faced foam insulation in the bays where the joists bear on the first-floor wall and seal the edges where the foam meets the framing with caulk or foam. Tape the joint where the poly on the first-floor wall face meets the foam between the joists.

Sealing Balloon-Framed Walls

Gable-end walls and shed dormer front walls are often balloon-framed. In these situations, heated air enters the wall through a penetration — such as an electrical outlet or even a crack around the baseboard and drywall at the bottom of the wall. The warm air rises in the stud cavity like smoke in a chimney, escaping into the cold attic and exiting through the roof vents. But even where there is no penetration in the wall, cold air from the attic will drop into the stud cavity where it is warmed by the wall and rises back into the attic. This kind of convection loop carries heat out of the house.

To prevent this type of heat loss, install wall blocking in line with the ceiling joists (**Figure 131**).

Sealing Framing Projections

Eyebrow roofs, bay window roofs, crickets, and other projections of the wall or roof lines are sometimes built

Figure 130. Cantilevers

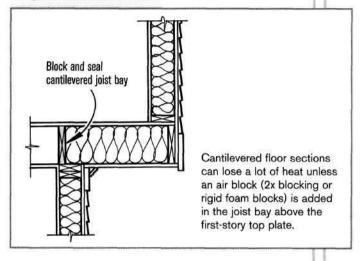
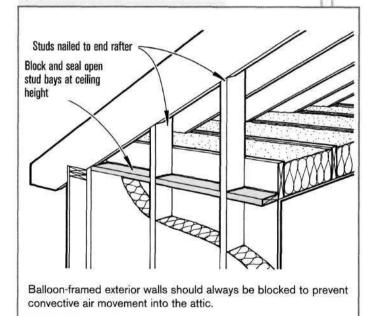
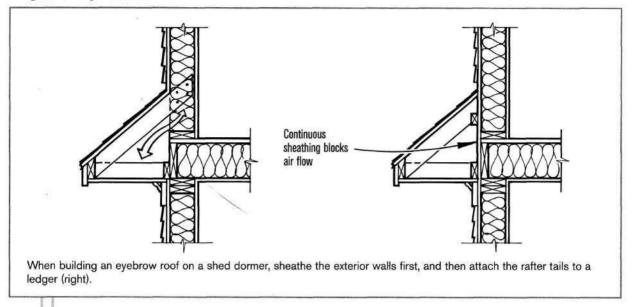


Figure 131. Balloon-Framed Walls



before the building is sheathed. This allows air to penetrate the exterior walls and leak out the building.

Figure 132. Eyebrow Roofs



To avoid these heat losses, always sheathe the exterior walls and then attach additional framing to a ledger (Figure 132).

Cathedral Ceiling Options

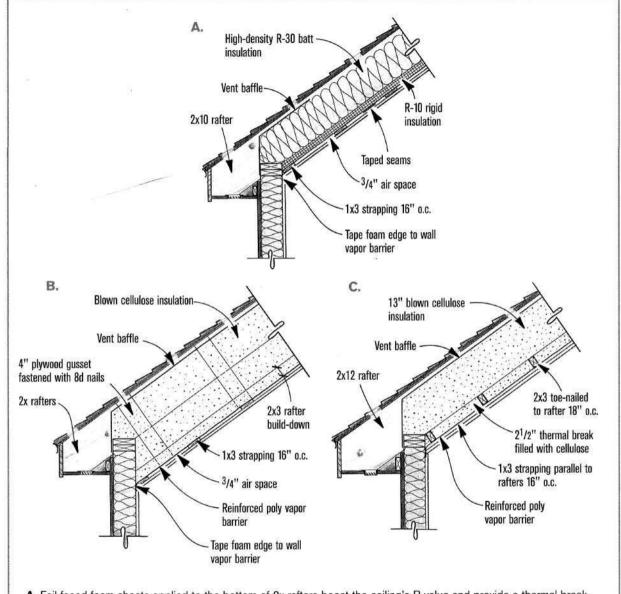
Cathedral ceilings must have adequate insulation (R-38 to R-40 in cold climates) and ventilation, but it can be a challenge to provide both in the space provided by a typical 12-in. rafter.

Hot vs. Cold Roofs

Most codes require new roofs to have an eaves-to-ridge flow of air. These are called *cold roofs* because they keep the underside of the sheathing cold in winter. In a heating climate, the flow of cold air under the sheathing discourages interior moisture buildup and ice damming. In a cooling climate, ventilation relieves heat buildup.

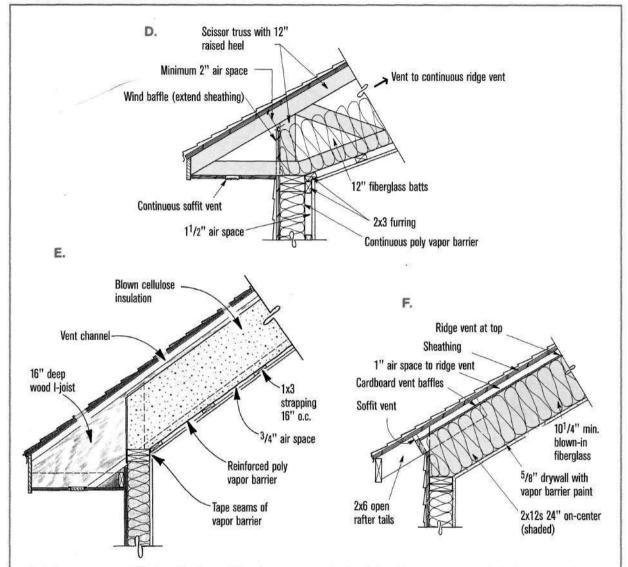
Cathedral ceilings that aren't ventilated are referred to as *hot roofs*, and typically rely on a well-sealed air and vapor barrier to keep moisture out of the roof. Solid-foam roof systems, using stress-skin panels or spray-in foam, are hot roof alternatives. However, many code officials do not permit these roofs. The cathedral ceiling options shown in this manual are all cold-roof options.

Figure 133. Cathedral Ceiling Options



- **A.** Foil-faced foam sheets applied to the bottom of 2x rafters boost the ceiling's R-value and provide a thermal break. Tape the seams between the foam sheets to reduce air and vapor movement into the ceiling cavity.
- B. Hang 2x3s below rafters using plywood gussets to create as wide a space as needed for blown cellulose insulation.
- C. Insulation space can be added by installing 2x3s toenailed across the bottom edge of the rafters, which also provides a thermal break.

Figure 133. Cathedral Ceiling Options, continued



- **D.** Scissors trusses with raised heels provide adequate space for insulation. Batts must be carefully fitted to minimize short-circuiting at truss chords.
- E. 16-in.-deep I-joists insulated with dense-blown cellulose.
- F. High R-value insulation (blown-in fiberglass) can be substituted for standard fiberglass batts or blown-in cellulose.

Cathedral Framing Options

Cathedral roofs framed with conventional 2x10 or 2x12 rafters typically do not provide adequate space for insulation in cold climates. The rafters need to be packed out to provide more space or foam insulation should be added to the underside (**Figure 133**, pages 85-86).

Thermal break. Since wood is not very good insulation, the rafters themselves conduct cold through the roof. Most of the framing options shown in Figure 133 provide a *thermal break*: an interruption of the conducting material (in this case, wood) intended to reduce continuous heat flow through the rafter.

Insulation options. The R-values of insulation materials vary widely, as shown in Figure 134, so installing insulation with a higher R-value may be the easiest alternative for cathedral ceilings. For example, high-performance batts or blown-in fiberglass (BIBS) can be used to bring the R-value of a 2x12 rafter space to an acceptable R-38 to R-40 (Figure 133, option F).

Vent baffle. In every cold-roof option shown in Figure 133, a vent baffle (using cardboard or vent channel) must be installed to provide uninterrupted airflow from eaves vents to a ridge vent.

Alternative Framing Options

An alternative to conventional rafters is to use scissors trusses or deep I-joists — these provide enough space for the extra insulation needed to achieve a higher R-value (**Figure 133**, options D and E).

Figure 134. Insulation R-Values

Insulation	Approx. R-Value per in.
Fiberglass batt	3.2
High-performance fiberglass batt	3.8
Loose-fill fiberglass	2.5
Blown-in fiberglass (BIBS)	4
Loose-fill cellulose	3.5
Dense-pack cellulose	3.5
Perlite or vermiculite	2.7
Expanded polystyrene board	3.8
Extruded polystyrene board	4.8
Foil-faced polyisocyanurate board	7
Spray-urethane foam	5.9

Steel in Wood Frames

Because of the high bearing capacity of steel, it is a useful alternative for carrying heavy loads, particularly where space is limited. Figure 135 shows the types of steel that can be useful for columns, beams, and brackets in wood-framed construction.

Figure 135. Steel Types and Sizes

	Shape & Ty	pe Symbol	Stock Size Specs	Lengths	Finish	Uses
I-Beams	Junior(1)	М	Height in inches	20, 40,	Hot-rolled,	Carrying beams,
Т	Standard	S	x pounds/LF	50, and	mill finish	headers, ridge beams
上	Wide Flange	W or WF	(Ex: W8x24)	60 feet		cantilevered beams
Channels	Stringer ⁽¹⁾	MC	Height in inches	20 and	Hot-rolled,	Carrying beams,
Г	Standard	C	x pounds/LF)	40 feet	mill finish	flitchplates, headers,
L	Ship & Car(2)	MC	(Ex: C5x9			ridge beams, columns
Tee	Tee(3)	T	Height in inches x width	20 feet	Hot-rolled,	Lintels, ledgers,
T			in inches (Ex: T6x8)		mill finish	light-load columns
Angles						
L	Equal Legs	Angle in degrees	Leg x leg x thickness	20 and	Hot-rolled,	Lintels, ledgers, web and
L_	Unequal Legs	or L	(Ex: 3x6x1/4")	40 feet	mill finish	flange reinforcements
			Gr.			joint clips
Bar Stock						
	Flats	N/A	Thickness x width (Ex: 1/2x8)	20 feet,	Hot-rolled, mill	Column plates,
•	Rounds		Diameter (Ex: 2")	12 feet and	finish Cold-rolled,	splice plates,
	Squares		Width of one side (Ex: 1")	random	pickled and oiled	machinist parts, tools
Pipe	Sch. 10 ⁽¹⁾	BPPE (black pipe	Inside diameter	21 to	Hot-rolled,	Columns
0	Sch. 40	plain end)or BPTC	x schedule weight	24 feet	mill finish,	
O	Sch. 80(2)	(black pipe	(3" Sch. 40 BPPE)		painted, hot galv.	
		threaded coupling)	MOR SCHOOLSTON CONTROLS TO CHOOLS		Jan Toronous year-our real authorises a section value	
Tubing			Outside dim. or diameter			
0	Round	ERW (elecres.	x wall thickness	20 and	Hot- or cold-rolled,	Handrails, balusters,
	Square	welded) DOM (drawn	(Ex: 2x ¹ /8" round;	40 feet	pickled and oiled	specialties
	Rectangular	over mandrel)	2x4x ¹ /4" rectangle)		0.000	098

⁽¹⁾ Also called "Lightweight"

Each grade of structural steel has a specific quality as described by American Society of Testing and Materials (ASTM) standards. ASTM A-326 is the predominant grade in the structural steel market. It has a carbon content of .26%, which gives it relatively high strength (60,000 psi tensile), yet it is relatively easy to weld and fabricate.

⁽²⁾ Also called "Heavyweight"

⁽³⁾ Made by splitting I-beams in half

Structural Steel Headers

Where height is limited, but a header must be installed to carry a heavy point load (a second-floor girder resting on a sliding-glass door header, for example), steel is often the only solution. Figure 136 shows examples of standard steel shapes and sizes that will work as headers to carry such heavy point loads. Each of these pieces of steel can be worked into a 2x4 wall, although the W beams (commonly called I-beams) are a full 4 in. wide and require careful work to fit.

Figure 136. Structural Steel Headers

		Sp	oan	
Point Load	i (lb.) 3'	4'	5'	6'
5,000	T3x3x ⁵ /16	T4x4x ³ /16	T4x3x1/4	C6x8.2
	(1.88)	(2.50)	(3.13)	(3.75)
10,000	C6x8.2	C6x10.5	W6x12	T6x3x ³ /8
	(3.75)	(5.00)	(6.25)	(7.50)
15,000	C6x13	T6x3x ³ /8	T7x3x ³ /8	W8x15
	(5.63)	(7.50)	(9.38)	(11.25)
20,000	T6x3x ³ /8	W6x16	W10x15	W10x17
	(7.50)	(10.00)	(13.00)	(15.00)
	T	С	W	R.
(Г		
	9 4			

The number in parentheses is the section modulus required for the given load and span; the steel section above it is the shallowest and lightest piece of steel that will work. Substitutions may have to be made because the steel yard may not carry every size and shape.

Figure 137. Splicing I-Beams

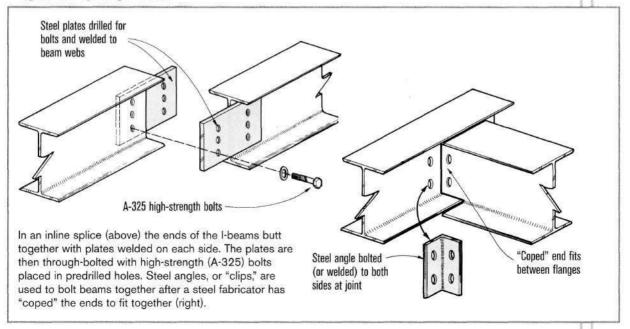
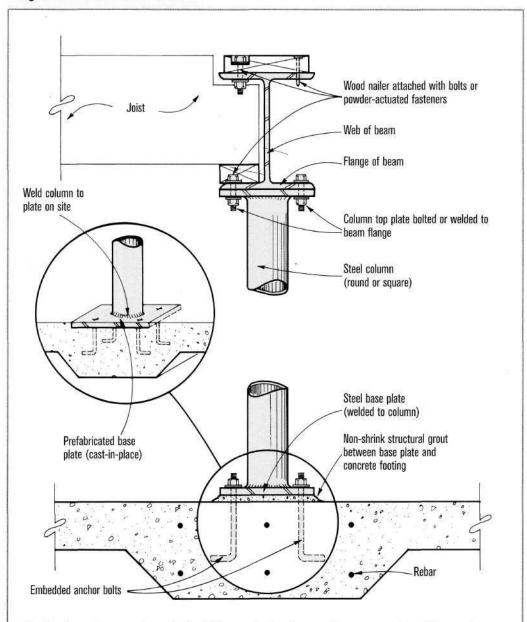


Figure 138. Column Connections



Steel columns (not wood posts) should be used when freestanding support of steel beams is required. The column plates must be bolted to beam flanges (top) and to the thickened slab footing (bottom). An alternative is to weld column plates to beam flanges, and weld column bases to steel base plates cast into the slab footings (inset).

Jack Support

Headers should be supported by at least double 2x4 jack studs for up to a 12,000-lb. load and triple jacks for loads above 12,000 lb. up to 18,000 lb. The header should sit directly on the end grain of the jack studs. Don't use wood shims under the header — the load is perpendicular to the grain and tends to crush the wood.

Steel-to-Steel Connections

Most steel connections are either bolted or welded together. Welding is useful when the surface area to be joined is small, such as the edge of a steel column.

Bolted connections, on the other hand, don't require special skills. The most common bolted connections are in-line splices and beam-to-beam connections at right angles (Figure 137, page 89), and where column plates join footings and beam flanges (Figure 138).

Right-angle connections (**Figure 137**, page 89) require the flange of one beam to be cut back ("coped") at one end so that the webs of each beam fit together. It doesn't have to be perfect, since the bolts will carry the load.

For any bolted structural connection, an engineer should specify the diameter and length of the bolts needed for the type of connection. These will probably be high-strength, structural steel (A-325) bolts, which are available from steel supply houses or steelwork shops.

Steel-to-Concrete Connections

Column bases must be bolted into concrete. Don't count on concrete alone to hold embedded steel in place. The concrete will shrink away over time, so you should attach the steel to anchor bolts. When embedding steel base plate for column supports, attach hooks to a portion of the steel that will be surrounded by concrete (inset, Figure 138). These will "grab" and prevent movement of the steel once the concrete has shrunk.

Steel-to-Wood Connections

There are several ways to attach steel to wood, depending on the circumstances. Figure 139, page 92 shows some common steel-to-wood connections using different steel shapes.

Nailers

Wood nailers are easiest to attach with powder-actuated nails, spaced 24- to 36-in. o.c. and staggered side-to-side.

Figure 139. Steel-to-Wood Connections

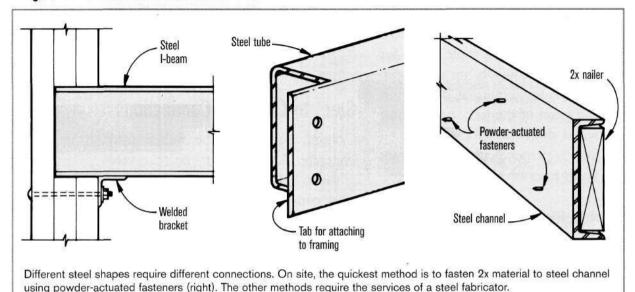
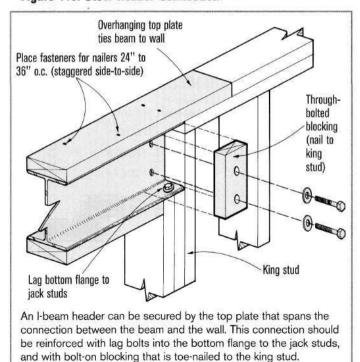


Figure 140. Steel Header Connection



Header Connections

A common way to attach an I-beam header to wood framing is to have the steel yard weld on an angle bracket, as shown in the left-hand illustration of Figure 139. An alternative is to secure the connection using a top plate, which overlaps the steel and wood-framed walls (Figure 140).

For slim-profile tube headers where there is not enough room to "nail on" lumber (using a powder-actuated tool), ask the steel fabricator to leave a tab sticking out at each end, as shown in the center illustration of **Figure 139**. Then notch the framing to fit, and nail or lag the steel to the framing.

Flitchplates

Flitchplates are used primarily in header assemblies when common framing lumber is not strong enough or stiff enough to carry the loads (**Figure 141**).

The steel is put in the middle for two reasons. First, this increases fire resistance. Wood can resist fire longer than steel, which softens very quickly in a fire. Second, the steel is not likely to buckle if placed between two wood members. A thin plate of steel will wrinkle and buckle under relatively small loads unless stabilized.

End Connections

An engineer should specify the size and number of bolts required to secure a flitch plate to the wood framing. Insufficient bolting and poorly sized bolt-holes will cause the wood around the bolts to crush and the plates to settle. In extreme cases, the steel can knife into the top of the post.

As a rule of thumb, bolt-holes should be placed 2 in. from all edges of a beam. Use the flitchplate as a template to precisely align the holes in the wood.

Figure 141. Equivalent Strengths: Flitch Beams vs. Built-Up Wood Beams & Steel I-Beams

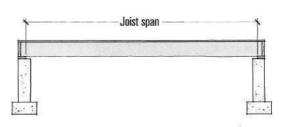
	Single Steel Flitch Beam	Built-Up Lumber Equivalents*	Steel I- Beam Equivalents
Wood	Steel		
2x6	5" x ¹ /4"	2.3 - 2x6s	-
	5 x ^{3/} 8	3.5 - 2x6s	-
	5 x ¹ / ₂	4.7 - 2x6s	-
2x8	7 x ¹ / ₄	2.8 - 2x8s	-
	7 x ³ /8	4.2 - 2x8s	-
	7 x ¹ /2	5.6 - 2x8s	W6x9
2x10	9 x ^{1/} 4	2.9 - 2x10s	-
	9 x ³ /8	4.3 - 2x10s	-
	9 x ¹ / ₂	5.8 - 2x10s	W8x10
2x12	11 x ¹ /4	2.9 - 2x12s	-
	11 x ³ /8	4.4 - 2x12s	=
	11 x ¹ /2	5.8 - 2x12s	W10x12

	Double Steel Flitch Beam	Built-Up Lumber Equivalents*	Steel I- Beam Equivalents
Wood	Steel		
2x6	5" x ¹ /4"	4.7 - 2x6s	-
	5 x ³ /8	7 - 2x6s	: =
	5 x ^{1/} 2	9.4 - 2x6s	i l Ti
2x8	7 x ¹ / ₄	5.6 - 2x8s	W6x9
	7 x ³ /8	8.4 - 2x8s	W8x10 or W6x12
	7 x ¹ /2	11.3 - 2x8s	W8x13
2x10	9 x ¹ / ₄	5.6 - 2x10s	W8x10
	9 x ³ /8	8.4 - 2x10s	W8x15
	9 x ¹ / ₂	11.5 - 2x10s	W8x18
2x12	11 x ¹ /4	5.8 - 2x12s	W10x12
	11 x ³ /8	8.8 - 2x12s	W10x17
	11 x ¹ /2	11.7 - 2x12s	W10x22

^{*} The strength equivalent shown for built-up lumber beams assumes Doug-fir-larch (E = 1.6, Fb = 1,200).

Figure 24. Maximum Allowable Spans (ft.-in.) for Floor Joists

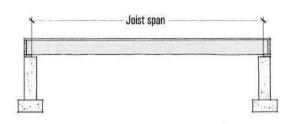




			2x6			2x8			2x10			2x12	
Species ! Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1	No. 2	No. 1-2 (Can.)
D-Fir-L	12	10-11	10-9	10-9	14-5	14-2	14-2	18-5	18-0	17-6	22-0	20-11	20-4
	16	9-11	9-9	9-9	13-1	12-9	12-5	16-5	15-7	15-2	19-1	18-1	17-7
	24	8-8	8-3	8-0	11-0	10-5	10-2	13-5	12-9	12-5	15-7	14-9	14-4
SPF	12	-	a—a	10-3	-	-	13-6	()— ()	-	17-3	: 	.—	20-7
	16	_	-	9-4	(—)	-	12-3	-	-	15-5	-	s — s	17-10
	24	1	5 — 5	8-1	3-3)	10-3	11-02	=	12-7	5 	(- -	14-7
Hem-Fir	12	10-6	10-0	10-9	13-10	13-2	14-2	17-8	16-10	18-0	21-6	20-4	21-11
	16	9-6	9-1	9-9	12-7	12-0	12-10	16-0	15-2	16-5	18-10	17-7	19-1
	24	8-4	7-11	8-6	10-10	10-2	11-0	13-3	12-5	13-5	15-5	14-4	15-7
SYP	12	10-11	10-9	-	14-5	14-2		18-5	18-0	-	22-5	21-9	47,00,07
	16	9-11	9-9	-	13-1	12-10	<u></u>	16-9	16-1	(5.7)	20-4	18-10	
	24	8-8	8-6	100	11-5	11-0	1036	14-7	13-2	A.	17-5	15-4	20 0

Figure 25. Maximum Allowable Spans (ft.-in.) for Floor Joists

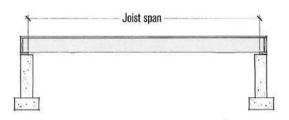
Residential Living Areas: 11/2-in. Concrete Floor (Tile Bed); 40 PSF Live, 20 PSF Dead (L/360)



5/			2x6			2x8			2x10			2x12	
Species Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1	No. 2	No. 1-2 (Can.)
D-Fir-L	12	10-11	10-8	10-4	14-2	13-6	13-1	17-4	16-5	16-0	20-1	19-1	18-6
	16	9-8	9-3	8-11	12-4	11-8	11-4	15-0	14-3	13-10	17-5	16-6	16-1
80	24	7-11	7-6	7-4	10-0	9-6	9-3	12-3	11-8	11-4	14-3	13-6	13-1
SPF	12	-	-	10-3	-	14-72	13-3	1	-	16-3	-	100	18-10
	16		892	9-1	150	Q=4	11-6	Store	-	14-1		309	16-3
	24	Ħ	East.	7-5	High	3323.	9-5	Name of the last o	100	11-6	-		13-4
Hem-Fir	12	10-6	10-0	10-9	13-10	13-1	14-2	17-1	16-0	17-4	19-10	18-6	20-1
	16	9-6	8-11	9-8	12-2	11-4	12-4	14-10	13-10	15-0	17-2	16-1	17-5
	24	7-10	7-4	7-11	9-11	9-3	10-0	12-1	11-4	12-3	14-0	13-1	14-3
SYP	12	10-11	10-9	3	14-5	14-2	-	18-5	16-11	S	22-5	19-10) -
	16	9-11	9-6	3	13-1	12-4	=	16-4	14-8	32	19-6	17-2	-
	24	8-8	7-9		11-3	10-0	-	13-4					

Figure 26. Maximum Allowable Spans (ft.-in.) for Ceiling Joists

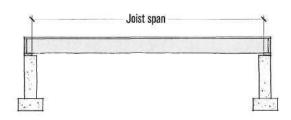
Drywall Attached - No Future Rooms and No Attic Storage; 10 PSF Live 5 PSF Dead (L/240)



			2x4			2x6			2x8			2x10	
Species S Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1	No. 2	No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1	No. 2	No. 1-2 (Can.)
D-Fir-L	12	12-8	12-5	12-5	19-11	19-6	19-6	26-2	25-8	25-8	33-5	32-9	32-0
	16	11-6	11-3	11-3	18-1	17-8	17-8	23-10	23-4	22-8	30-0	28-6	27-8
	24	10-0	9-10	9-10	15-9	15-0	14-7	20-1	19-1	18-6	24-6	23-3	22-7
SPF	12	9 	03 9	11-10	20—20	_	18-8	70-0	(-)	24-7	S-3	0 — 0	31-4
	16	-); — ;	10-9		-	16-11	80 — 83	2-00	22-4	::—::	0;=0	28-1
	24	3 - 0	35 — 3	9-5	::	_	14-9	11-11	8 - 08	18-9	-	31—3	22-11
Hem-Fir	12	12-2	11-7	12-5	19-1	18-2	19-6	25-2	24-0	25-8	32-1	30-7	32-9
	16	11-0	10-6	11-3	17-4	16-6	17-8	22-10	21-9	23-4	29-2	27-8	29-9
	24	9-8	9-2	9-10	15-2	14-5	15-6	19-10	18-6	20-1	24-3	22-7	24-6
SYP	12	12-8	12-5	-	19-11	19-6	-	26-2	25-8	X 37	33-5	32-9	-
	16	11-6	11-3	3 - 2	18-1	17-8	-	23-10	23-4	4 3- 8	30-5	29-4	
	24	10-0	9-10	1 21	15-9	15-6	-	20-10	20-1	36 -1 88	26-6	24-0	-
										Sinter or an arrangement			

Figure 27. Maximum Allowable Spans (ft.-in.) for Ceiling Joists

Drywall Attached - No Future Rooms, Limited Attic Storage; 20 PSF Live 10 PSF Dead (L/240)



			2x4			2x6			2x8			2x10	
Species : Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1	No. 2	No. 1-2 (Can.)
D-Fir-L	12	10-0	9-10	9-10	15-9	15-0	14-7	20-1	19-1	18-6	24-6	23-3	22-7
	16	9-1	8-11	8-8	13-9	13-0	12-8	17-5	16-6	16-0	21-3	20-2	19-7
	24	7-8	7-3	7-1	11-2	10-8	10-4	14-2	13-6	13-1	17-4	16-5	16-0
SPF	12	#	-	9-5	-	-	14-9	-		18-9		-	22-11
	16	-	-	8-7	=	-	12-10	-	8	16-3		-	19-10
	24		-	7-2	-	-	10-6	-	-	13-3		-	16-3
Hem-Fir	12	9-8	9-2	9-10	15-2	14-5	15-6	19-10	18-6	20-1	24-3	22-7	24-6
	16	8-9	8-4	8-11	13-7	12-8	13-9	17-2	16-0	17-5	21-0	19-7	21-3
	24	7-7	7-1	7-8	11-1	10-4	11-2	14-0	13-1	14-2	17-1	16-0	17-4
SYP	12	10-0	9-10	120	15-9	15-6	*	20-10	20-1	<u></u>	26-6	24-0	-
	16	9-1	8-11	-	14-4	13-6	-	18-11	17-5	=	23-2	20-9	37 <u></u> 3
	24	8-0	7-8	-	12-6	11-0	8 — 8	15-11	14-2	=	18-11	17-0	2=2

Maximum

Header

Size 2-2x4

2-2x6

2-2x8

2-2x10

2-2x12

3-2x8

3-2x10

3-2x12

4-2x8

4-2x10

4-2x12

20

1

2

2

1

1

1

1

3-6

5-5

6-10

8-5

9-9

8-4

10-6

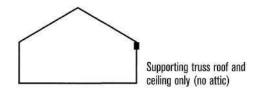
12-2

9-2

11-8

14-1

Figure 60. Header and Girder Spans (ft.-in.) for Exterior Bearing Walls



20 lb. Snow Load **Building Width (ft.)**

2-10

4-2

5-4

6-6

7-6

6-8

8-2

9-5

7-8

9-5

10-11

36

Span No. of Jacks Span No. of Jacks 1 1 2 2 2 1 2

2

2

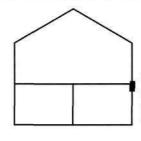
2

2

50 lb. Snow Load Building Width (ft.)

m	20	3	36
Span	No. of Jacks	Span	No. of Jacks
2-10	1	2-2	1
4-1	1	3-2	2
5-2	2	4-0	2
6-4	2	4-11	2
7-4	2	5-8	3
6-6	2	5-0	2
7-11	2	6-2	2
9-2	2	7-2	2
7-6	2	5-10	2
9-2	2	7-1	2
10-8	2	8-3	2
	2-10 4-1 5-2 6-4 7-4 6-6 7-11 9-2 7-6 9-2	Span No. of Jacks 2-10 1 4-1 1 5-2 2 6-4 2 7-4 2 6-6 2 7-11 2 9-2 2 7-6 2 9-2 2	Span No. of Jacks Span 2-10 1 2-2 4-1 1 3-2 5-2 2 4-0 6-4 2 4-11 7-4 2 5-8 6-6 2 5-0 7-11 2 6-2 9-2 2 7-2 7-6 2 5-10 9-2 2 7-1

Figure 61. Header and Girder Spans (ft.-in.) for Exterior Bearing Walls



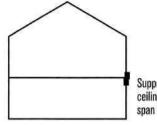
Supporting truss roof and ceiling (no attic) + one center-bearing floor and

20 lb. Snow Load **Building Width (ft.)**

50 lb. Snow Load **Building Width (ft.)**

Maximur Header	n	20	3	36	Maximu Header	ım	20	;	36
Size	Span	No. of Jacks	Span	No. of Jacks	Size	Span	No. of Jacks	Span	No. of Jacks
2-2x4	3-1	21	2-5	1	2-2x4	2-6	1	2-0	1
2-2x6	4-6	1	3-7	2	2-2x6	3-8	1	2-11	2
2-2x8	5-9	2	4-6	2	2-2x8	4-8	2	3-8	2
2-2x10	7-0	2	5-6	2	2-2x10	5-8	2	4-5	2
2-2x12	8-1	2	6-5	2	2-2x12	6-7	2	5-2	2
3-2x8	7-2	1	5-8	2	3-2x8	5-10	1	4-7	2
3-2x10	8-9	2	6-11	2	3-2x10	7-1	2	5-7	2
3-2x12	10-2	2	8-0	2	3-2x12	8-3	2	6-6	2
4-2x8	8-1	2	6-7	2	4-2x8	6-8	2	5-3	2
4-2x10	10-1	1	8-0	2	4-2x10	8-2	2	6-5	2
4-2x12	11-9	2	9-3	2	4-2x12	9-6	2	7-6	2
					_				

Figure 62. Header and Girder Spans (ft.-in.) for Exterior Bearing Walls



Supporting truss roof and ceiling (no attic) + clearspan floor and ceiling

20 lb. Snow Load Building Width (ft.)

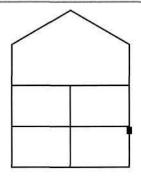
50 lb. Snow Load Building Width (ft.)

36

Maximu Header	m	20	3	36	Maximu Header	m	20
Size	Span	No. of Jacks	Span	No. of Jacks	Size	Span	No.
2-2x4	2-8	1	2-1	1	2-2x4	2-5	
2-2x6	3-11	1	3-0	2	2-2x6	3-6	
2-2x8	5-0	2	3-10	2	2-2x8	4-5	
2-2x10	6-1	2	4-8	2	2-2x10	5-5	
2-2x12	7-1	2	5-5	3	2-2x12	6-3	
3-2x8	6-3	2	4-10	2	3-2x8	5-6	/// //a
3-2x10	7-7	2	5-11	2	3-2x10	6-9	
3-2x12	8-10	2	6-10	2	3-2x12	7-10	
4-2x8	7-2	2	5-7	2	4-2x8	6-4	
4-2x10	8-9	2	6-10	2	4-2x10	7-9	
4-2x12	10-2	2	7-11	2	4-2x12	9-0	

Header								
Size	Span	No. of Jacks	Span	No. of Jacks				
2-2x4	2-5	1	1-10	1				
2-2x6	3-6	2	2-9	2				
2-2x8	4-5	2	3-5	2				
2-2x10	5-5	2	4-3	3				
2-2x12	6-3	2	4-11	3				
3-2x8	5-6	2	4-4	2				
3-2x10	6-9	2	5-3	2				
3-2x12	7-10	2	6-1	2				
4-2x8	6-4	2	5-0	2				
4-2x10	7-9	2	6-1	2				
4-2x12	9-0	2	7-1	2				

Figure 63. Header and Girder Spans (ft.-in.) for Exterior Bearing Walls



Supporting truss roof and ceiling (no attic) + two center-bearing floors and ceilings

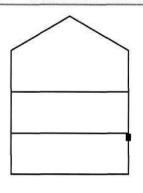
20 lb. Snow Load Building Width (ft.)

50 lb. Snow Load Building Width (ft.)

Maximum Header		20	36			
Size	Span	No. of Jacks	Span	No. of Jacks		
2-2x4	2-7	1	2-0	1		
2-2x6	3-9	2	2-11	2		
2-2x8	4-9	2	3-9	2		
2-2x10	5-9	2	4-7	3		
2-2x12	6-8	2	5-3	3		
3-2x8	5-11	2	4-8	2		
3-2x10	7-3	2	5-9	2		
3-2x12	8-5	2	6-7	2		
4-2x8	6-10	2	5-5	2		
4-2x10	8-4	2	6-7	2		
4-2x12	9-8	2	7-8	2		

Maximum Header		20	3	36
Size	Span	No. of Jacks	Span	No. of Jacks
2-2x4	2-3	1	1-10	1
2-2x6	3-4	2	2-8	2
2-2x8	4-3	2	3-4	2
2-2x10	5-2	2	4-1	3
2-2x12	6-0	2	4-9	3
3-2x8	5-4	2	4-2	2
3-2x10	6-6	2	5-2	2
3-2x12	7-6	2	6-0	3
4-2x8	6-1	2	4-10	2
4-2x10	7-6	2	5-11	2
4-2x12	8-8	2	6-11	2

Figure 64. Header and Girder Spans (ft.-in.) for Exterior Bearing Walls



Supporting truss roof and ceiling (no attic) + two clear-span floors and ceilings

20 lb. Snow Load Building Width (ft.)

Maximum 20 36 Header Span No. of Jacks Span No. of Jacks Size 2-2x4 2-1 1-7 2 1 3-1 2-2x6 2 2-4 2 2-2x8 3-10 2 3-0 3 2 2-2x10 4-9 3-8 3 5-6 3 2-2x12 4-3 3 3-2x8 4-10 2 2 3-9 3-2x10 5-11 2 4-7 3 3-2x12 6-10 2 3 5-4

2

2

2

5-7

6-10

7-11

4-2x8

4-2x10

4-2x12

50 lb. Snow Load Building Width (ft.)

		10000			
n	20	36			
Span	No. of Jacks	Span	No. of Jacks		
2-0	1	1-7	2		
2-11	2	2-3	2		
3-9	2	2-11	3		
4-7	2	3-6	3		
5-3	3	4-1	3		
4-8	. 2	3-7	2		
5-8	2	4-5	3		
6-7	2	5-1	3		
5-5	2	4-2	3		
6-7	2	5-1	2		
7-8	2	5-11	3		
	Span 2-0 2-11 3-9 4-7 5-3 4-8 5-8 6-7 5-5 6-7	Span No. of Jacks 2-0 1 2-11 2 3-9 2 4-7 2 5-3 3 4-8 2 5-8 2 6-7 2 5-5 2 6-7 2	Span No. of Jacks Span 2-0 1 1-7 2-11 2 2-3 3-9 2 2-11 4-7 2 3-6 5-3 3 4-1 4-8 2 3-7 5-8 2 4-5 6-7 2 5-1 5-5 2 4-2 6-7 2 5-1		

Note: Calculated spans assume #2 grade Doug.-Fir, Hem-Fir and SYP lumber.

4-4

5-3

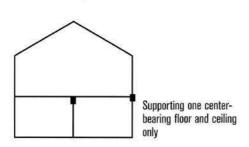
6-2

3

2

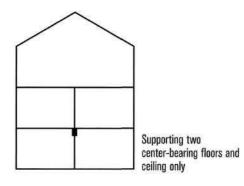
3

Figure 65. Header and Girder Spans (ft.-in.) for Interior Bearing Walls



20 lb. Snow Load Building Width (ft.)

Maximum Header		20	3	36
Size	Span	No. of Jacks	Span	No. of Jacks
2-2x4	3-5	1	2-6	1
2-2x6	4-11	1	3-8	1
2-2x8	6-3	1	4-8	2
2-2x10	7-8	2	5-9	2
2-2x12	8-11	2	6-7	2
3-2x8	7-10	1	5-10	2
3-2x10	9-7	1	7-2	2
3-2x12	11-1	2	8-3	2
4-2x8	9-0	1	6-9	2
4-2x10	11-1	1	8-3	2
4-2x12	12-10	1	9-7	2



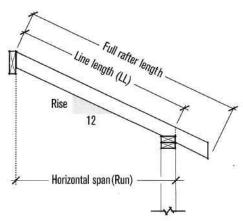
50 lb. Snow Load

Building Width (ft.)

Maximum Header		20	3	36					
Size	Span	No. of Jacks	Span	No. of Jacks					
2-2x4	2-3	1	1-9	1					
2-2x6	3-4	2	2-6	2					
2-2x8	4-3	2	3-3	2					
2-2x10	5-2	2	3-11	3					
2-2x12	6-0	2	4-7	3					
3-2x8	5-4	2	4-0	2					
3-2x10	6-6	2	4-11	2					
3-2x12	7-6	2	5-8	3					
4-2x8	6-1	2	4-8	2					
4-2x10	7-6	2	5-8	2					
4-2x12	8-8	2	6-7	2					

Figure 69. Maximum Allowable Horizontal Spans (ft.-in.)

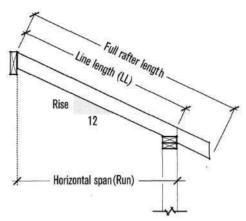
Rafters: 20 psf live load; 10 psf dead load. Non-snow region. Lightweight roof covering. No ceiling drywall.



		2x4			2x6			2x8			2x10	
Spacing (in.)	No. 1-2 No. 1 No. 2 (Can.)		No. 1	No. 1-2 No. 1 No. 2 (Can.)		No. 1-2 No. 1 No. 2 (Can.)			No. 1-2 No. 1 No. 2 (Can.)			
12	11-1	10-10	10-10	17-4	16-10	16-4	22-5	21-4	20-8	27-5	26-0	25-3
16	10-0	9-10	9-8	15-4	14-7	14-2	19-5	18-5	17-11	23-9	22-6	21-11
24	8-7	8-2	7-11	12-6	11-11	11-7	15-10	15-1	14-8	19-5	18-5	17-10
12	-	_	10-4	_	0-0	16-3	-	-	21-0	-	-	25-8
16	-	3-	9-5	-	10-0	14-4	_	-	18-2	-	-	22-3
24		-	8-0	(pp)	20 -0 3	11-9	(==	=	14-10	=	(===	18-2
12	10-7	10-1	10-10	16-8	15-11	17-0	21-11	20-8	22-5	27-1	25-3	27-5
16	9-8	9-2	9-10	15-2	14-2	15-4	19-2	17-11	19-5	23-5	21-11	23-9
24	8-5	7-11	8-7	12-4	11-7	12-6	15-8	14-8	15-10	19-2	17-10	19-5
12	11-1	10-10	-	17-4	17-0	\$ - 8	22-11	22-5	-	29-2	26-9	-
16	10-0	9-10		15-9	15-1	à - 8	20-10	19-6	-	25-10	23-2	(-)
24	8-9	8-7	100	13-9	12-4	0 N - 10	17-9	15-11	-	21-1	18-11	-
	(in.) 12 16 24 12 16 24 12 16 24 12 16 24 16	(in.) No. 1 12 11-1 16 10-0 24 8-7 12 - 16 - 24 - 12 10-7 16 9-8 24 8-5 12 11-1 16 10-0	Figure (in.) No. 1 No. 2 12 11-1 10-10 16 10-0 9-10 24 8-7 8-2 12 16 24 12 10-7 10-1 16 9-8 9-2 24 8-5 7-11 12 11-1 10-10 16 10-0 9-10	Spacing (in.) No. 1 No. 2 (Can.) 12 11-1 10-1010-10 16 10-0 9-10 9-8 24 8-7 8-2 7-11 12 - - 10-4 16 - - 9-5 24 - - 8-0 12 10-7 10-1 10-10 16 9-8 9-2 9-10 24 8-5 7-11 8-7 12 11-1 10-10 - 16 10-0 9-10 -	Spacing (in.) No. 1 No. 2 (Can.) No. 1 12 11-1 10-1010-10 17-4 16 10-0 9-10 9-8 15-4 24 8-7 8-2 7-11 12-6 12 - - 10-4 - 16 - - 9-5 - 24 - - 8-0 - 12 10-7 10-1 10-10 16-8 16 9-8 9-2 9-10 15-2 24 8-5 7-11 8-7 12-4 12 11-1 10-10 - 17-4 16 10-0 9-10 - 15-9	Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 12 11-1 10-1010-10 17-4 16-10 16 10-0 9-10 9-8 15-4 14-7 24 8-7 8-2 7-11 12-6 11-11 12 - - 10-4 - - 16 - - 9-5 - - 24 - - 8-0 - - 12 10-7 10-1 10-10 16-8 15-11 16 9-8 9-2 9-10 15-2 14-2 24 8-5 7-11 8-7 12-4 11-7 12 11-1 10-10 - 17-4 17-0 12 11-1 10-10 - 17-4 17-0 16 10-0 9-10 - 15-9 15-1	Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 1 (Can.) No. 1 No. 2 (Can.) 12 11-1 10-10 10-10 17-4 16-10 16-4 16 10-0 9-10 9-8 15-4 14-7 14-2 24 8-7 8-2 7-11 12-6 11-11 11-7 12 - - 10-4 - - 16-3 16 - - 9-5 - - 14-4 24 - - 8-0 - - 11-9 12 10-7 10-1 10-10 16-8 15-11 17-0 16 9-8 9-2 9-10 15-2 14-2 15-4 24 8-5 7-11 8-7 12-4 11-7 12-6 12 11-1 10-10 - 17-4 17-0 - 16 10-0 9-10 - 15-9 15-1 - <td>Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 12 11-1 10-1010-10 17-4 16-10 16-4 22-5 16 10-0 9-10 9-8 15-4 14-7 14-2 19-5 24 8-7 8-2 7-11 12-6 11-11 11-7 15-10 12 - - 10-4 - - 16-3 - 16 - - 9-5 - - 14-4 - 24 - - 8-0 - - 11-9 - 12 10-7 10-1 10-10 16-8 15-11 17-0 21-11 16 9-8 9-2 9-10 15-2 14-2 15-4 19-2 24 8-5 7-11 8-7 12-4 11-7 12-6 15-8 12 11-1 10-10 - 17-4</td> <td>Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 No. 1 No. 1 No. 2 No. 1 No. 1<td>Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1 No. 1-2 (Can.) 12 11-1 10-10 10-10 17-4 16-10 16-4 22-5 21-4 20-8 16 10-0 9-10 9-8 15-4 14-7 14-2 19-5 18-5 17-11 24 8-7 8-2 7-11 12-6 11-11 11-7 15-10 15-1 14-8 12 - - 10-4 - - 16-3 - - 21-0 16 - - 9-5 - - 14-4 - - 18-2 24 - - 8-0 - - 11-9 - - 14-10 12 10-7 10-1 10-10 16-8 15-11 17-0 21-11 20-8 22-5 16 9-8 9-2 9-10 15-2<td>Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1</td><td>Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 No. 2 No. 1 No. 2 Can.) No. 2 Can.) No. 1 No. 1 No. 2 Can.) No. 1 No. 1 No. 1 No. 1 No</td></td></td>	Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 12 11-1 10-1010-10 17-4 16-10 16-4 22-5 16 10-0 9-10 9-8 15-4 14-7 14-2 19-5 24 8-7 8-2 7-11 12-6 11-11 11-7 15-10 12 - - 10-4 - - 16-3 - 16 - - 9-5 - - 14-4 - 24 - - 8-0 - - 11-9 - 12 10-7 10-1 10-10 16-8 15-11 17-0 21-11 16 9-8 9-2 9-10 15-2 14-2 15-4 19-2 24 8-5 7-11 8-7 12-4 11-7 12-6 15-8 12 11-1 10-10 - 17-4	Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 No. 1 No. 1 No. 2 No. 1 No. 1 <td>Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1 No. 1-2 (Can.) 12 11-1 10-10 10-10 17-4 16-10 16-4 22-5 21-4 20-8 16 10-0 9-10 9-8 15-4 14-7 14-2 19-5 18-5 17-11 24 8-7 8-2 7-11 12-6 11-11 11-7 15-10 15-1 14-8 12 - - 10-4 - - 16-3 - - 21-0 16 - - 9-5 - - 14-4 - - 18-2 24 - - 8-0 - - 11-9 - - 14-10 12 10-7 10-1 10-10 16-8 15-11 17-0 21-11 20-8 22-5 16 9-8 9-2 9-10 15-2<td>Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1</td><td>Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 No. 2 No. 1 No. 2 Can.) No. 2 Can.) No. 1 No. 1 No. 2 Can.) No. 1 No. 1 No. 1 No. 1 No</td></td>	Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1 No. 1-2 (Can.) 12 11-1 10-10 10-10 17-4 16-10 16-4 22-5 21-4 20-8 16 10-0 9-10 9-8 15-4 14-7 14-2 19-5 18-5 17-11 24 8-7 8-2 7-11 12-6 11-11 11-7 15-10 15-1 14-8 12 - - 10-4 - - 16-3 - - 21-0 16 - - 9-5 - - 14-4 - - 18-2 24 - - 8-0 - - 11-9 - - 14-10 12 10-7 10-1 10-10 16-8 15-11 17-0 21-11 20-8 22-5 16 9-8 9-2 9-10 15-2 <td>Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1</td> <td>Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 No. 2 No. 1 No. 2 Can.) No. 2 Can.) No. 1 No. 1 No. 2 Can.) No. 1 No. 1 No. 1 No. 1 No</td>	Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1	Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 No. 2 No. 1 No. 2 Can.) No. 2 Can.) No. 1 No. 1 No. 2 Can.) No. 1 No. 1 No. 1 No. 1 No

Figure 70. Maximum Allowable Horizontal Spans (ft.-in.)

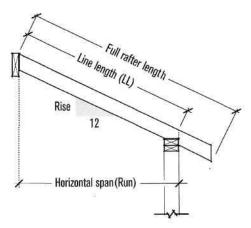
Rafters: 20 psf live load; 10 psf dead load. Non-snow region. Light-weight roof covering. Drywall ceiling. No Attic.



			2x6			2x8			2x10			2x12	
Species Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1	No. 2	No. 1-2 (Can.)
D-Fir-L	12	15-9	15-6	15-6	20-10	20-5	20-5	26-6	26-0	25-3	31-10	30-2	29-4
	16	14-4	14-1	14-1	18-11	18-5	17-11	23-9	22-6	21-11	27-6	26-1	25-5
	24	12-6	11-11	11-7	15-10	15-1	14-8	19-5	18-5	17-10	22-6	21-4	20-9
SPF	12	-	-	14-9	-	-	19-6	-	-	24-10	-	-	29-9
	16	-	-	13-5	-	-	17-9	=	-	22-3	-	=	25-9
	24	-		11-9	-	<u> </u>	14-10	(-4)	1	18-2	-		21-0
Hem-Fir	12	15-2	14-5	15-6	19-11	19-0	20-5	25-5	24-3	26-0	30-11	29-4	31-8
	16	13-9	13-1	14-1	18-2	17-3	18-6	23-2	21-11	23-8	27-2	25-5	27-6
	24	12-0	11-5	12-3	15-8	14-8	15-10	19-2	17-10	19-5	22-2	20-9	22-6
SYP	12	15-9	15-6		20-10	20-5	-	26-6	26-0	_	32-3	31-4	
	16	14-4	14-1	-	18-11	18-6	_	24-1	23-2	9 - 9	29-4	27-2	122
	24	12-6	12-3		16-6	15-11		21-1	18-11		25-2	22-2	<u> </u>

Figure 71. Maximum Allowable Horizontal Spans (ft.-in.)

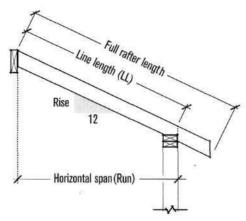
Rafters: 20 psf live load; 10 psf dead load. Snow region. Light-weight roof covering. No ceiling drywall.



			2x4			2x6			2x8			2x10	
Species S Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)
D-Fir-L	12	11-1	10-10	10-9	17-0	16-2	15-8	21-6	20-5	19-10	26-4	24-11	24-3
	16	10-0	9-7	9-3	14-9	14-0	13-7	18-8	17-8	17-2	22-9	21-7	21-0
	24	8-3	7-10	7-7	12-0	11-5	11-1	15-3	14-5	14-0	18-7	17-8	17-2
SPF	12	-	XX - 03	10-4	-	-	15-11	(-)	-	20-2	-	(- 0	24-7
	16	-	-	9-5	-	-	13-9	-	4	17-5	-	10-01	21-4
	24	-	S 39	7-8	-	-	11-3	1 - 2	-	14-3	-	3,-3	17-5
Hem-Fir	12	10-7	10-1	10-10	16-8	15-8	17-0	21-3	19-10	21-6	26-0	24-3	26-4
	16	9-8	9-2	9-10	14-6	13-7	14-9	18-5	17-2	18-8	22-6	21-0	22-9
	24	8-1	7-7	8-3	11-10	11-1	12-0	15-0	14-0	15-3	18-4	17-2	18-7
SYP	12	11-1	10-10	-	17-4	16-8	(.—»	22-11	21-7	1000	28-7	25-8	-
8	16	10-0	9-10	-	15-9	14-5) n - e	20-10	18-8	-	24-9	22-3	_
	24	8-9	8-2	AD	13-6	11-9	-	17-0	15-3		20-3	18-2	

Figure 72. Maximum Allowable Horizontal Spans (ft.-in.)

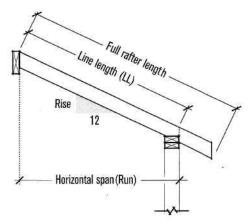
Rafters: 20 psf live load; 10 psf dead load. Snow region. Lightweight roof covering. Drywall ceiling. No Attic.



			2x6			2x8			2x10			2x12	
Species S Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)
D-Fir-L	12	15-9	15-6	15-6	20-10	20-5	19-10	26-4	24-11	24-3	30-6	28-11	28-1
	16	14-4	14-0	13-7	18-8	17-8	17-2	22-9	21-7	21-0	26-5	25-1	24-4
ijt.	24	12-0	11-5	11-1	15-3	14-5	14-0	18-7	17-8	17-2	21-7	20-5	19-11
SPF	12	-	1-	14-9	-	778	19-6	()_ /)	=	24-7	-	-	28-6
9	16		2	13-5	=	-3	17-5	-	=	21-4	-	-	24-8
	24	1887	-	11-3	=	=	14-3	-	-	17-5	-	-	20-2
Hem-Fir	12	15-2	14-5	15-6	19-11	19-0	20-5	25-5	24-3	26-0	30-1	28-1	30-6
	16	13-9	13-1	14-1	18-2	17-2	18-6	22-6	21-0	22-9	26-1	24-4	26-5
	24	11-10	11-1	12-0	15-0	14-0	15-3	18-4	17-2	18-7	21-3	19-11	21-7
SYP	12	15-9	15-6		20-10	20-5	()	26-6	25-8	100	32-3	30-1	-94
	16	14-4	14-1	#	18-11	18-6	-	24-1	22-3	200	29-4	26-1	=
	24	12-6	11-9		16-6	15-3	-	20-3	18-2		24-1	21-4	-

Figure 73. Maximum Allowable Horizontal Spans (ft.-in.)

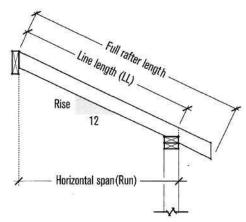
Rafters: 30 psf live load; 10 psf dead load. Snow region. Lightweight roof covering. No ceiling drywall.



			2x4			2x6			2x8			2x10	
Species S Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)
D-Fir-L	12	9-8	9-6	9-3	14-9	14-0	13-7	18-8	17-8	17-2	22-9	21-7	21-0
	16	8-9	8-3	8-0	12-9	12-1	11-9	16-2	15-4	14-11	19-9	18-9	18-2
	24	7-1	6-9	6-7	10-5	9-10	9-7	13-2	12-6	12-2	16-1	15-3	14-10
SPF	12	-	_	9-1	-	-	13-9	-	Ø — 3	17-5	(S —)	-	21-4
	16	4 1 - 8	 :	8-2	10-0	-	11-11	ma t	:-:	15-1	×=:	-	18-5
	24	1 - 0	7.7 2	6-8	-	-	9-9	=	-	12-4	(-)	_	15-1
Hem-Fir	12	9-3	8-10	9-6	14-6	13-7	14-9	18-5	17-2	18-8	22-6	21-0	22-9
	16	8-5	8-0	8-7	12-7	11-9	12-9	15-11	14-11	16-2	19-6	18-2	19-9
	24	7-0	6-7	7-1	10-3	9-7	10-5	13-0	12-2	13-2	15-11	14-10	16-1
SYP	12	9-8	9-6	-	15-2	14-5	-	20-0	18-8	1 18 1	24-9	22-3	
	16	8-9	8-7	-	13-9	12-6	(171	18-0	16-2	a = 8	21-5	19-3	-
	24	7-8	7-1	1	11-9	10-2	. 	14-9	13-2	8 - 8	17-6	15-9	-
				200									

Figure 74. Maximum Allowable Horizontal Spans (ft.-in.)

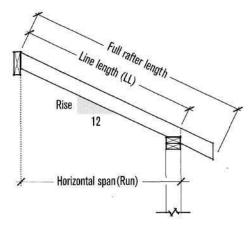
Rafters: 30 psf live load; 10 psf dead load. Snow region. Lightweight roof covering. Drywall ceiling. No Attic.



			2x6			2x8			2x10			2x12	
Species : Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1	No. 2	No. 1-2 (Can.)
D-Fir-L	12	13-9	13-6	13-6	18-2	17-8	17-2	22-9	21-7	21-0	26-5	25-1	24-4
	16	12-6	12-1	11-9	16-2	15-4	14-11	19-9	18-9	18-2	22-10	21-8	21-1
	24	10-5	9-10	9-7	13-2	12-6	12-2	16-1	15-3	14-10	18-8	17-9	17-3
SPF	12	-	-	12-11	-	-	17-0	H	-	21-4	-	-	24-8
	16	1,500	-	11-9	-	-	15-1	-	22	18-5	-	-	21-5
	24	-	-	9-9	-		12-4	74	-	15-1	-	(8_0)	17-6
Hem-Fir	12	13-3	12-7	13-6	17-5	16-7	17-10	22-3	21-0	22-9	26-1	24-4	26-5
	16	12-0	11-5	12-3	15-10	14-11	16-2	19-6	18-2	19-9	22-7	21-1	22-10
	24	10-3	9-7	10-5	13-0	12-2	13-2	15-11	14-10	16-1	18-5	17-3	18-8
SYP	12	13-9	13-6	=	18-2	17-10	2004	23-2	22-3	5 <u></u>	28-2	26-1	<u></u>
	16	12-6	12-3	-	16-6	16-2	<u></u>	21-1	19-3	-	25-7	22-7	
	24	10-11	10-2	-	14-5	13-2	-	17-6	15-9	-	20-10	18-5	_

Figure 75. Maximum Allowable Horizontal Spans (ft.-in.)

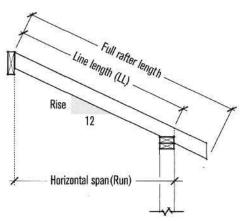
Rafters: 30 psf live load; 20 psf dead load. Snow region. Heavy roof covering. No ceiling drywall.



			2x4			2x6			2x8			2x10	
Species S Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)
D-Fir-L	12	9-0	8-6	8-4	13-2	12-6	12-2	16-8	15-10	15-4	20-4	19-4	18-9
5	16	7-10	7-5	7-2	11-5	10-10	10-6	14-5	13-8	13-4	17-8	16-9	16-3
	24	6-4	6-0	5-10	9-4	8-10	8-7	11-9	11-2	10-10	14-5	13-8	13-3
SPF	12	-	=======================================	8-5		=	12-4	<u>- 100</u>	=	15-7	<u>au</u>	222	19-1
	16	-	_	7-3	200	-	10-8	==	=	13-6	2020)		16-6
	24	W <u>-6</u> 3	444	5-11	=	-	8-9	<u>mer</u>		11-0	=	-	13-6
Hem-Fir	12	8-11	8-4	9-0	13-0	12-2	13-2	16-6	15-4	16-8	20-1	18-9	20-4
	16	7-8	7-2	7-10	11-3	10-6	11-5	14-3	13-4	14-5	17-5	16-3	17-8
	24	6-3	5-10	6-4	9-2	8-7	9-4	11-8	10-10	11-9	14-3	13-3	14-5
SYP	12	9-8	9-0	2000	14-10	12-11	-	18-8	16-8	<u> </u>	22-2	19-11	-
	16	8-8	7-9	 3	12-10	11-2	-	16-2	14-5	-	19-2	17-3	(-)
	24	7-1	6-4	-	10-6	9-1	394-00	13-2	11-10	e -	15-8	14-1	-

Figure 76. Maximum Allowable Horizontal Spans (ft.-in.)

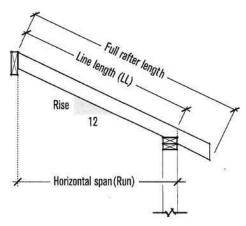
Rafters: 30 psf live load; 20 psf dead load. Snow region. Heavy roof covering. Drywall ceiling. No Attic.



			2x6			2x8			2x10	(4)		2x12	
Species S Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)
D-Fir-L	12	13-2	12-6	12-2	16-8	15-10	15-4	20-4	19-4	18-9	23-7	22-5	21-9
	16	11-5	10-10	10-6	14-5	13-8	13-4	17-8	16-9	16-3	20-5	19-5	18-10
	24	9-4	8-10	8-7	11-9	11-2	10-10	14-5	13-8	13-3	16-8	15-10	15-5
SPF	12	-	-	12-4	-		15-7	-	1	19-1	-	(-)	22-1
	16		1-1	10-8	-		13-6	-	-	16-6	-	-	19-2
	24	200	-	8-9	-		11-0	-	2	13-6	-	-	15-7
Hem-Fir	12	13-0	12-2	13-2	16-6	15-4	16-8	20-1	18-9	20-4	23-4	21-9	23-7
	16	11-3	10-6	11-5	14-3	13-4	14-5	17-5	16-3	17-8	20-2	18-10	20-5
	24	9-2	8-7	9-4	11-8	10-10	11-9	14-3	13-3	14-5	16-6	15-5	16-8
SYP	12	13-9	12-11	-	18-2	16-8		22-2	19-11	-	26-5	23-4	=
	16	12-6	11-2	(<u>=</u>)	16-2	14-5		19-2	17-3	-	22-10	20-2	
	24	10-6	9-1	_	13-2	11-10		15-8	14-1	7 — 7	18-8	16-6	

Figure 77. Maximum Allowable Horizontal Spans (ft.-in.)

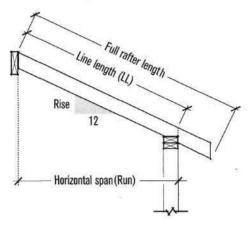
Rafters: 40 psf live load; 10 psf dead load. Snow-region. Lightweight roof covering. No ceiling drywall.



			2x4			2x6			2x8			2x10	
Species S Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)
D-Fir-L	12	8-9	8-6	8-4	13-2	12-6	12-2	16-8	15-10	15-4	20-4	19-4	18-9
	16	7-10	7-5	7-2	11-5	10-10	10-6	14-5	13-8	13-4	17-8	16-9	16-3
	24	6-4	6-0	5-10	9-4	8-10	8-7	11-9	11-2	10-10	14-5	13-8	13-3
SPF	12	-	=	8-3	=	<u>.</u> -0	12-4	-	-	15-7		-	19-1
	16	(-)		7-3		-	10-8	=	=	13-6	-	#	16-6
	24	×=1	122	5-11	-	-	8-9	=	-	11-0	200	-	13-6
Hem-Fir	12	8-5	8-0	8-7	13-0	12-2	13-2	16-6	15-4	16-8	20-1	18-9	20-4
	16	7-8	7-2	7-10	11-3	10-6	11-5	14-3	13-4	14-5	17-5	16-3	17-8
	24	6-3	5-10	6-4	9-2	8-7	9-4	11-8	10-10	11-9	14-3	13-3	14-5
SYP	12	8-9	8-7	=	13-9	12-11	=	18-2	16-8	<u> </u>	22-2	19-11	(* <u>—</u> **)
	16	8-0	7-9	_	12-6	11-2	(<u>-</u>	16-2	14-5	=	19-2	17-3	_
4	24	7-0	6-4	_	10-6	9-1	16-	13-2	11-10	(i) <u></u> (15-8	14-1	-

Figure 79. Maximum Allowable Horizontal Spans (ft.-in.)

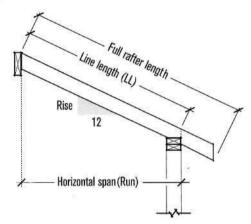
Rafters: 40 psf live load; 15 psf dead load. Snow region. Medium-weight roof covering. No ceiling drywall.



2x10	
No. 2	No. 1-2 (Can.)
18-5	17-11
15-11	15-6
13-0	12-8
-	18-2
-	15-9
_	12-10
17-11	19-5
15-6	16-10
12-8	13-9
19-0	-
16-5	e-:
13-5	
	15-6 12-8 19-0 16-5

Figure 80. Maximum Allowable Horizontal Spans (ft.-in.)

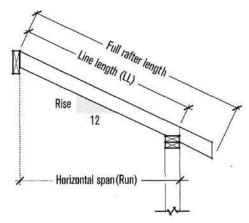
Rafters: 40 psf live load; 15 psf dead load. Snow region. Medium-weight roof covering. Drywall ceiling, No Attic.



			2x6			2x8			2x10			2x12	Į.
Species Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1	No. 2	No. 1-2 (Can.)
D-Fir-L	12	12-6	11-11	11-7	15-11	15-1	14-8	19-5	18-5	17-11	22-6	21-4	20-9
	16	10-10	10-4	10-0	13-9	13-1	12-8	16-10	15-11	15-6	19-6	18-6	18-0
	24	8-11	8-5	8-2	11-3	10-8	10-4	13-9	13-0	12-8	15-11	15-1	14-8
SPF	12	-	-	11-9	-		14-10	1	-	18-2	=	-	21-1
	16	- 18	-	10-2	-		12-11	- "	=	15-9	-	-	18-3
	24	V <u>575</u>	-	8-4	87 <u>—</u> 57		10-6	_	-	12-10	<u> </u>	(<u>—</u>)	14-11
Hem-Fir	12	12-0	11-5	12-3	15-8	14-8	15-11	19-2	17-11	19-5	22-3	20-9	22-6
	16	10-9	10-0	10-10	13-7	12-8	13-9	16-7	15-6	16-10	19-3	18-0	19-6
	24	8-9	8-2	8-11	11-1	10-4	11-3	13-7	12-8	13-9	15-9	14-8	15-11
SYP	12	12-6	12-3	_	16-6	15-11	_	21-1	19-0	: 	25-2	22-3	
	16	11-5	10-8	: <u></u>	15-0	13-9	-	18-3	16-5	-	21-9	19-3	1 20)
	24	9-11	8-8	-	12-7	11-3	-	14-11	13-5	:—	17-9	15-9	

Figure 81. Maximum Allowable Horizontal Spans (ft.-in.)

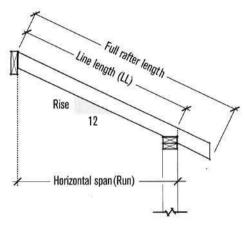
Rafters: 50 psf live load; 10 psf dead load. Snow region. Lightweight roof covering. Drywall ceiling. No Attic.



		2x6			2x8			2x10			2x12	
Spacing (in.)	No. 1			No. 1			No. 1	0.850 59	(6255.0) (CAC)	No. 1	No. 2	No. 1-2 (Can.)
12	11-8	11-5	11-1	15-3	14-5	14-0	18-7	17-8	17-2	21-7	20-5	19-11
16	10-5	9-10	9-7	13-2	12-6	12-2	16-1	15-3	14-10	18-8	17-9	17-3
24	8-6	8-1	7-10	10-9	10-3	9-11	13-2	12-6	12-1	15-3	14-6	14-1
12	-	(1 -1)	10-11	-	-	14-3	-	2 — 0	17-5	-	10—10	20-2
16	-	-	9-9	7 — 8	_	12-4	-	-	15-1	: - 0	·	17-6
24	-	0-0	7-11	: - :	-	10-1	-	-	12-4	3-2	10 -1 0	14-3
12	11-2	10-8	11-5	14-8	14-0	15-0	18-4	17-2	18-7	21-3	19-11	21-7
16	10-2	9-7	10-4	13-0	12-2	13-2	15-11	14-10	16-1	18-5	17-3	18-8
24	8-5	7-10	8-6	10-8	9-11	10-9	13-0	12-1	13-2	15-1	14-1	15-3
12	11-8	11-5	(- 0	15-4	15-0	_	19-7	18-2	-	23-9	21-4	-
16	10-7	10-2	-	13-11	13-2	-	17-6	15-9		20-10	18-5	-
24	9-3	8-4	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	12-0	10-9	J-16	14-4	12-10	Same .	17-0	15-1	-
	(in.) 12 16 24 12 16 24 12 16 24 12 16 24 16	(in.) No. 1 12 11-8 16 10-5 24 8-6 12 - 16 - 24 - 12 11-2 16 10-2 24 8-5 12 11-8 16 10-7	Spacing (in.) No. 1 No. 2 12 11-8 11-5 16 10-5 9-10 24 8-6 8-1 12 16 24 12 11-2 10-8 16 10-2 9-7 24 8-5 7-10 12 11-8 11-5 16 10-7 10-2	Spacing (in.) No. 1 No. 2 (Can.) 12 11-8 11-5 11-1 16 10-5 9-10 9-7 24 8-6 8-1 7-10 12 - - 10-11 16 - - 9-9 24 - - 7-11 12 11-2 10-8 11-5 16 10-2 9-7 10-4 24 8-5 7-10 8-6 12 11-8 11-5 - 16 10-7 10-2 -	Spacing (in.) No. 1 No. 2 (Can.) No. 1 12 11-8 11-5 11-1 15-3 16 10-5 9-10 9-7 13-2 24 8-6 8-1 7-10 10-9 12 - - 10-11 - 16 - - 9-9 - 24 - - 7-11 - 12 11-2 10-8 11-5 14-8 16 10-2 9-7 10-4 13-0 24 8-5 7-10 8-6 10-8 12 11-8 11-5 - 15-4 16 10-7 10-2 - 13-11	Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 12 11-8 11-5 11-1 15-3 14-5 16 10-5 9-10 9-7 13-2 12-6 24 8-6 8-1 7-10 10-9 10-3 12 - - 10-11 - - 16 - - 9-9 - - 24 - - 7-11 - - 12 11-2 10-8 11-5 14-8 14-0 16 10-2 9-7 10-4 13-0 12-2 24 8-5 7-10 8-6 10-8 9-11 12 11-8 11-5 - 15-4 15-0 16 10-7 10-2 - 13-11 13-2	Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 1-2 (Can.) 12 11-8 11-5 11-1 15-3 14-5 14-0 16 10-5 9-10 9-7 13-2 12-6 12-2 24 8-6 8-1 7-10 10-9 10-3 9-11 12 - - 10-11 - - 14-3 16 - - 9-9 - - 10-1 12 11-2 10-8 11-5 14-8 14-0 15-0 16 10-2 9-7 10-4 13-0 12-2 13-2 24 8-5 7-10 8-6 10-8 9-11 10-9 12 11-8 11-5 - 15-4 15-0 - 16 10-7 10-2 - 13-11 13-2 -	Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 1 </td <td>Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 No. 1 No. 1 No. 2 No. 1 No. 2</td> <td>Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1-2 (Can.) No. 1-2 (Can.) No. 1-2 (Can.) No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1<!--</td--><td>Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1 No. 1-2 (Can.) No. 1 No.</td><td>Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 Can.) No. 1 No. 2 No</td></td>	Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 No. 1 No. 1 No. 2 No. 1 No. 2	Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1-2 (Can.) No. 1-2 (Can.) No. 1-2 (Can.) No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1 No. 1-2 (Can.) No. 1 No. 1 </td <td>Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1 No. 1-2 (Can.) No. 1 No.</td> <td>Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 Can.) No. 1 No. 2 No</td>	Spacing (in.) No. 1 No. 1-2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1-2 (Can.) No. 1 No. 1 No. 1 No. 1-2 (Can.) No. 1 No.	Spacing (in.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 (Can.) No. 1 No. 2 Can.) No. 1 No. 2 No

Figure 82. Maximum Allowable Horizontal Spans (ft.-in.)

Rafters: 50 psf live load; 15 psf dead load. Snow region. Medium-weight roof covering. Drywall ceiling. No Attic.



			2x6			2x8			2x10			2x12	
Species S Group	Spacing (in.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1		No. 1-2 (Can.)	No. 1	No. 2	No. 1-2 (Can.)
D-Fir-L	12	11-7	10-11	10-8	14-7	13-10	13-6	17-10	16-11	16-6	20-9	19-8	19-1
	16	10-0	9-6	9-3	12-8	12-0	11-8	15-6	14-8	14-3	17-11	17-0	16-6
	24	8-2	7-9	7-6	10-4	9-10	9-6	12-8	12-0	11-8	14-8	13-11	13-6
SPF	12		\ - 2	10-10	9,79	1657	13-8	/I=	-	16-9	9=38	-	19-5
	16	-	=	9-4	-		11-10	-		14-6	-	-	16-9
	24	-	-3	7-8) -		9-8	=	-	11-10	-	=8	13-8
Hem-Fir	12	11-2	10-8	11-5	14-5	13-6	14-7	17-8	16-6	17-10	20-5	19-1	20-9
	16	9-10	9-3	10-0	12-6	11-8	12-8	15-3	14-3	15-6	17-9	16-6	17-11
	24	8-1	7-6	8-2	10-3	9-6	10-4	12-6	11-8	12-8	14-6	13-6	14-8
SYP	12	11-8	11-4	F=3	15-4	14-8		19-5	17-6	15 — 16	23-2	20-6	_
	16	10-7	9-10	1=1	13-11	12-8	_	16-10	15-1	5 — 5	20-0	17-9	
	24	9-2	8-0	23—23	11-7	10-4	_	13-9	12-4	13—1	16-4	14-6	-

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